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June 29, 1981

Mr. Joe Watts  
Mail Stop 160A  
NASA Langley Research Center  
Hampton, VA 23665

Dear Joe:

Enclosed are the original and two (2) copies of my research report, "An Exploratory Investigation of Weight Estimation Techniques for Hypersonic Flight Vehicles." I am also sending two (2) copies to the NASA Scientific and Technical Information Facility. Our research office also asked me to enclose an invention declaration. If there is anything else that should be done, please let me know.

Sincerely yours,

A handwritten signature in cursive script, reading "Everett L. Cook".

Everett L. Cook  
Adjunct Associate Professor

ELC/dg

(NASA-CR-164420) AN EXPLORATORY  
INVESTIGATION OF WEIGHT ESTIMATION  
TECHNIQUES FOR HYPERSONIC FLIGHT VEHICLES  
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INVENTION DECLARATION

There were no inventions discovered in the course of the  
research sponsored by NASA under Cooperative Agreement No. NCCI-21.

*Everett L. Cook*

Everett L. Cook  
Principal Investigator



# AN EXPLORATORY INVESTIGATION OF WEIGHT ESTIMATION TECHNIQUES FOR HYPERSONIC FLIGHT VEHICLES

by Everett L. Cook  
Wichita State University

## INTRODUCTION

Studies to determine the feasibility of hypersonic aircraft (refs. 1-4) require a reliable method of weight prediction. This report discusses the three basic methods of weight prediction and some of the computer programs that have been developed to implement them. The need for a data base of component weights is also discussed.

The WAATS program (ref. 5) was chosen as the best readily available program for use in design studies of hypersonic aircraft. The program was modified to improve its performance. The modified program is presented, along with newly devised input data forms and an example problem.

## METHODS OF WEIGHT PREDICTION

The categories of weight prediction methods are not clearly defined; and there is always overlap in any categorization. In this report, the methods will be defined as:

1. The Fixed-Fraction Method.
2. The Statistical Correlation Method.
3. The Point Stress Analysis Method.

The methods are listed in increasing order of complexity, and each method has an area of applicability. Roland (ref. 6) discusses the three methods, using different terminology, and presents flow charts that indicate their relative complexity.

### The Fixed-Fraction Method

This method is very simple; the weights of the vehicle components are assumed to be a fixed-fraction of the empty weight or takeoff weight. It is only valid when the vehicle being designed

is only a slight variation of an existing design. Gersh and York (ref. 7) give an example of this method and discuss the pitfalls. The weight of the Hypersonic Transport (HST) used as an example to demonstrate the use of the WAATS program is largely determined by this method (ref. 8).

Caddell (ref. 9) presents a variation of the fixed-fraction method that is based on the relationship between the structural weight and the aircraft density.

#### The Statistical Correlation Method

The Statistical Correlation Method is the most widely used of the three methods. Many of the weight prediction procedures use this method entirely, and most of the Point Stress Analysis programs use statistical correlation for some component weights. The method is based on correlating historical weight data using a simple equation, usually

$$W = \sum A_i X_i^{B_i} \quad (1)$$

where  $W$  is the component weight,

$A_i$  is an empirically determined weight coefficient,

$B_i$  is an empirically determined exponent,

$X_i$  is a parameter.

The selection of the parameters,  $X_i$ , is the key to the success of obtaining good correlation. They may consist of one or more characteristics of the component or the vehicle. For instance, the wing weight equation used in the WAATS program is of the form

$$W = A_1(W_{TO} \cdot n \cdot b_{ST} \cdot S/t_R)^{B_1} + A_2 \cdot S + A_3 + A_4(W_{LDG} \cdot n \cdot b_{ST} \cdot S/t_R)^{B_4} \quad (2)$$

where  $W_{TO}$  is the takeoff weight,

$W_{LDG}$  is the landing weight,

$n$  is the ultimate wing load factor,

$b_{ST}$  is the structural span.

$S$  is the wing area,

$t_R$  is the wing thickness at the root.

The first and last parameters are the same except for the weights; so that the wing weight can be based on the most critical condition, takeoff or landing. Since the parameter does contain a vehicle weight ( $W_{TO}$  or  $W_{LDG}$ ), the procedure is iterative. The other characteristics in  $X_1$  and  $X_4$  are derived from the loads ( $n$ ) and the geometry ( $b_{GT}$ ,  $S$  and  $t_R$ ). The selection of these characteristics should be based on an approximate analysis of the component, where this is possible. Dimensional analysis may frequently be used to determine nondimensional combinations of the characteristics. The second and third terms in Eq. 2 ( $B_2 = 1.0$  and  $B_3 = 0.0$ ) allow the inclusion of weight items that vary with the wing area or are fixed, respectively.

The number of equations used in a statistical correlation weight estimation procedure may vary from less than ten (ref. 10) to several hundred (ref. 6). Increasing the number of equations does not automatically increase the accuracy of the weight estimation procedure. However, the ability to predict the effects of technology advances is enhanced as the number of equations increases.

The Fixed-Fraction Method is a special case of this method, with all  $B_i = 1.0$  and all of the parameters  $X_i$  equal to a vehicle weight.

The Space Shuttle Synthesis Program--SSSP (ref. 11), the Weights Analysis of Advanced Transportation Systems program--WAATS (ref. 5), and the Systems Engineering Mass Properties program--SEMP (ref. 12) are NASA developed statistical correlation programs for advanced transportation systems. As indicated by its name, SSSP was developed to predict the weight of the Space Shuttle. The WAATS program was developed from SSSP to permit weight prediction for a wider range of high speed vehicles. The SEMP program was developed specifically for Earth-to-orbit vehicles, and thus is more general than SSSP, but not as general as WAATS.

Gersch and York (ref. 7) describe a statistical correlation program, WISE-ONE, which is used in the early phase of preliminary design at Grumman. It provides the capability of examining a large number of designs in this phase. To complement the tabulated output data, it generates a printer-plot of the configuration.

In addition to descriptions of programs based on the statistical correlation method, the literature also contains information on specific component weight estimation techniques. The Papers of the Society of Allied Weight Engineers are an excellent source of information of this type. Some examples are:

Fuselage Structure. -- Simpson (ref. 13) discusses an analytical method and computer program for fuselage structure weight prediction. Equations are given for various items (floors, pressure bulkheads, doors, windows, etc.).

Thermal Protection Systems. -- Roland (ref. 14) presents techniques for calculating the unit weights of two types of heat shields and the thickness and weight of bulk insulation. Fessenden (ref. 15) discusses both passive and active thermal protection systems and presents equations for calculating unit weights.

Engines. -- Klees and Fishbach (ref. 16) present a method of estimating both the dimensions and the weight of gas turbine engines. They demonstrate the method with a detailed example problem.

Propellant Tanks and Systems. -- Conrad (ref. 17) discusses the effects of tank construction on the weight of propulsion systems using cryogenic liquids. Equations for tank thicknesses and weights and pressurization gas and system weights are given. Willoughby (ref. 18) presents a semi-empirical method for calculating tank weights for nine common configurations. Both pump-fed and pressure-fed pressurization systems are also considered.

Systems and Equipment. -- Roland (ref. 6) presents 132 equations for predicting the weights of various aircraft systems and equipment items. He also presents correlation curves for many of the equations.

#### The Point Stress Analysis Method

The Point Stress Analysis method, as such, is only applicable to the major structural components of the vehicle, i.e., the wing, tail, fuselage, landing gear, etc. The weight estimate is based on the material required to carry the loads at representative "points" in the component. This requires the specification of both the component loads and the allowable stresses. Due to the complexity of this method, a computer program is a necessity. The weights of the nonstructural items are normally calculated with statistical correlation equations.

The majority of the programs in this category have been developed by individual aerospace companies and are proprietary. However, the Structural WEight Estimation Program--SWEEP (ref. 19)

was developed by Rockwell International for the Air Force and is available from the Air Force Flight Dynamics Laboratory. It was developed for military aircraft weight estimation (cargo, fighter, fighter bomber and attack bomber), so modifications would be required to adapt it to weight estimation for hypersonic aircraft.

In addition to the statistical correlation program, WISE-ONE, Gersch and York (ref. 7) also describe Grumman's WISE-TWO program which uses the point stress analysis method to calculate the wing and tail weights. Although this program does not use point stress analysis for the fuselage, it has an option to stretch or shrink the fuselage to accommodate the required fuel load.

The literature also contains some information on point stress analysis weight estimation techniques for individual components, but the number of papers is not as great as for statistical correlation methods. Two examples are:

Fuselage Structure. -- Staton (ref. 20) presents a FORTRAN program for calculating the basic shell weight for an unpressurized fuselage. The weight penalties associated with the design features are discussed and an example for a typical fighter/attack airplane is given.

Landing Gear. -- Kraus (ref. 21) describes a computer program which can be used to estimate the weight of aircraft landing gear. The loads are first calculated and then the strut member sizes are estimated.

#### DATA BASE

The requirement for reliable weight estimation procedures for all classes of flight vehicles will continue to exist as long as these vehicles are being designed. And the verification of these procedures will continue to be based on historical data. Thus, a comprehensive data base of component weights would be invaluable to weight engineers involved in advancing weight estimation technology. NASA could make a significant contribution to this field by sponsoring a project to compile such a data base and make it available to the aerospace industry.

#### THE WAATS PROGRAM

WAATS--Weights Analysis of Advanced Transportation Systems--was developed (ref. 5) to provide a program that could be used either with the ODIN--Optimal Design INtegration--System or as a

stand-alone program. It uses the statistical correlation method and relies heavily on the equations developed for the Space Shuttle Synthesis Program--SSSP (ref. 11). However, a number of equations are included which did not come from the SSSP.

Of the readily available programs, WAATS appeared to be the only one that could be used for hypersonic aircraft feasibility studies without major modification. When an attempt was made to implement the program using the listing in ref. 5, a number of minor errors were discovered. Further investigation revealed that the program could be made more efficient by recoding. The modified program is given with a discussion of the modifications to each subroutine. This is followed by a description of the input data and a set of newly devised input data forms that should make the program easier to use. Finally, an example problem is presented to demonstrate the use of the program.

#### Main Program

The main program is essentially the same as the original--the four primary subroutines (DATA, INPUT, MASS and PRINT) are called, with all of the data being transferred through named common blocks. However, some of the common block and subroutine names have been changed. The dimensions have also been changed and are transmitted to the subroutines through the new common block, SIZES. The input and output unit numbers are also transmitted through common, so only the main program has to be changed when the dimensions or input and output numbers have to be changed.



C	MAIN PROGRAM WAATS-C - NOVEMBER 1980	WAATS001
C	.....	WAATS002
C		WAATS003
C	PURPOSE	WAATS004
C	WEIGHTS ANALYSIS FOR ADVANCED TRANSPORTATION SYSTEMS.	WAATS005
C		WAATS006
C	REMARKS	WAATS007
C	THIS PROGRAM IS A MODIFICATION OF R.C. GLATT'S, 'WAATS - A	WAATS008
C	COMPUTER PROGRAM FOR WEIGHTS ANALYSIS OF ADVANCED TRANS-	WAATS009
C	PORTATION SYSTEMS.' NASA CR-2420, SEPTEMBER 1974.	WAATS010
C		WAATS011
C	SUBPROGRAMS REQUIRED	WAATS012
C	DATA, INPUT, MASS, ATMOS AND PRINT.	WAATS013
C	.....	WAATS014
C		WAATS015
C	SPECIFICATION STATEMENTS.	WAATS016
C	COMMON /INPUT/ NR,NW	WAATS017
	COMMON /SIZES/ KIC,KC,KAC,KW	WAATS018
	COMMON /INTGR/ IC(3)	WAATS019
	COMMON /COMON/ C(42)	WAATS020
	COMMON /ACDEF/ AC(134)	WAATS021
	COMMON /WAITS/ W(74)	WAATS022
		WAATS023
C	DEFINE THE INPUT AND OUTPUT UNITS.	WAATS024
C	NR=1	WAATS025
	NW=4	WAATS026
		WAATS027
C	DEFINE THE ARRAY DIMENSIONS.	WAATS028
C	KIC=3	WAATS029
	KC=42	WAATS030
	KAC=134	WAATS031
	KW=74	WAATS032
		WAATS033
C	CALL THE SUBROUTINES.	WAATS034
C	CALL DATA	WAATS035
	CALL INPUT	WAATS036
	CALL MASS	WAATS037
	CALL PRINT	WAATS038
	CALL EXIT	WAATS039
	END	WAATS040

### Subroutine DATA

This subroutine still performs the same basic purpose as the original, i.e., the initialization of the design data (IC and C), the weight coefficients and exponents (AC) and the weights (W). However, there are several major changes:

1. All initialization is done with arithmetic statements, instead of a combination of arithmetic and data statements.
2. The real design data (C) is first set to 0.0. Selected values are then specified. The specified values are given both in the WAATS Design Data listing and Input Data form.
3. The weight coefficient and exponents are also initially set to 0.0 and then selected values are specified. The specified values are based on a study of the equations in ref. 5. In cases where there were more than one equation; high speed, rocket powered aircraft were taken as the reference.

The component weights are all set to 0.0, as in the original subroutine.

C	SUBROUTINE DATA	DATA0001
C	.....	DATA0002
C		DATA0003
C	PURPOSE	DATA0004
C	INITIALIZE THE DESIGN DATA, THE WEIGHT COEFFICIENTS AND	DATA0005
C	EXPONENTS, AND THE WEIGHTS.	DATA0006
C		DATA0007
C	USAGE	DATA0008
C	CALL DATA	DATA0009
C		DATA0010
C	REMARKS	DATA0011
C	THE OUTPUT IS THROUGH THE COMMON BLOCKS. THE INTEGER	DATA0012
C	DESIGN DATA IS SPECIFIED. THE REAL DESIGN DATA AND THE	DATA0013
C	WEIGHT COEFFICIENTS AND EXPONENTS ARE FIRST SET TO 0.0.	DATA0014
C	SELECTED DESIGN DATA AND WEIGHT COEFFICIENTS AND EXPONENTS	DATA0015
C	ARE THEN SPECIFIED. THE EXPONENTS NOT OTHERWISE SPECIFIED	DATA0016
C	ARE SET TO 1.0E-6. ALL OF THE WEIGHTS ARE SET TO 0.0.	DATA0017
C		DATA0018
C	SUBPROGRAMS REQUIRED	DATA0019
C	NONE	DATA0020
C	.....	DATA0021
C		DATA0022
C	SPECIFICATION STATEMENTS.	DATA0023
C	COMMON /SIZES/ KIC,KC,KAC,KW	DATA0024
	COMMON /INTGR/ IC(3)	DATA0025
	COMMON /CCMON/ C(42)	DATA0026
	COMMON /ACDEF/ AC(134)	DATA0027
	COMMON /WAITS/ W(74)	DATA0028
	EQUIVALENCE (IC(1),ICRY ),(IC(2),IENG ),(IC(3),ISHAPE)	DATA0029
	EQUIVALENCE (C( 1),ACTR ),(C( 2),AICAPT),(C( 3),ARATIO),	DATA0030
1	(C( 4),CREW ),(C( 5),DH ),(C( 6),DM ),	DATA0031
2	(C( 7),ELBODY),(C( 8),ELNLET),(C( 9),ELRAMP),	DATA0032
3	(C(10),ENGIN),(C(11),FCTMOK),(C(12),GEOFCT),	DATA0033
4	(C(13),GSPAN ),(C(14),HBODY ),(C(15),OF ),	DATA0034
5	(C(16),OFACS ),(C(17),PCHAM ),(C(18),PHIGH ),	DATA0035
6	(C(19),PLOW ),(C(20),QMAX ),(C(21),SBODY ),	DATA0036
4	(C(22),SFAIR ),(C(23),SFUTK ),(C(24),SHORZ ),	DATA0037
8	(C(25),SOXTK ),(C(26),STPS ),(C(27),STSPAN),	DATA0038
9	(C(28),SVERT ),(C(29),SWING ),(C(30),TANKS ),	DATA0039
	EQUIVALENCE (C(31),THRUST),(C(32),TROOT ),(C(33),TYTAIL),	DATA0040

1	(C(34),VFUTK ),(C(35),VOXTK ),(C(36),WAREF ),	DATA0041
2	(C(37),WLANDI),(C(38),WPAYLD),(C(39),WPMAIN),	DATA0042
3	(C(40),WTOIN ),(C(41),XINLET),(C(42),XLF )	DATA0043
C		DATA0044
C	INITIALIZE THE INTEGER DESIGN DATA.	DATA0045
	ICRY=2	DATA0046
	IENG=3	DATA0047
	ISHAPE=2	DATA0048
C		DATA0049
C	INITIALIZE THE REAL DESIGN DATA.	DATA0050
	DO 2 I=1,KC	DATA0051
2	C(I)=0.0	DATA0052
	ACTR=1.0	DATA0053
	CREW=2.0	DATA0054
	DM=1.0	DATA0055
	ENGINS=2.0	DATA0056
	FC TMOK=1.0	DATA0057
	GEOFCT=1.0	DATA0058
	HBODY=1.0	DATA0059
	QF=6.0	DATA0060
	PCHAM=1000.0	DATA0061
	PHIGH=176.0	DATA0062
	PLGW=46.0	DATA0063
	TANKS=1.0	DATA0064
	TYTAIL=1.25	DATA0065
	XINLET=1.0	DATA0066
	XLF=4.0	DATA0067
C		DATA0068
C	INITIALIZE THE WEIGHT COEFFICIENTS AND EXPONENTS.	DATA0069
	DO 4 I=1,KAC	DATA0070
4	AC(I)=0.0	DATA0071
	AC( 1)=2505.0	DATA0072
	AC( 4)=5.0	DATA0073
	AC( 6)=0.00035	DATA0074
	AC( 15)=0.341	DATA0075
	AC( 17)=0.98	DATA0076
	AC( 19)=0.0025	DATA0077
	AC( 25)=0.31	DATA0078
	AC( 28)=0.00766	DATA0079
	AC( 29)=0.00033	DATA0080

AC( 30)=0.5  
 AC( 31)=130.0  
 AC( 32)=1782.63  
 AC( 33)=0.003  
 AC( 34)=1594.53  
 AC( 35)=0.0032  
 AC( 36)=0.53  
 AC( 38)=1.25  
 AC( 40)=0.59  
 AC( 42)=0.23  
 AC( 50)=0.45  
 AC( 51)=2.45  
 AC( 53)=4.345  
 AC( 54)=1.0  
 AC( 57)=78.5  
 AC( 58)=0.079  
 AC( 60)=0.323  
 AC( 64)=0.10  
 AC( 66)=1.167  
 AC( 68)=2.64  
 AC( 70)=66.37  
 AC( 72)=220.0  
 AC( 78)=0.608  
 AC( 81)=1.0  
 AC( 82)=0.1  
 AC( 89)=1.09  
 AC( 90)=1.0  
 AC(101)=0.795  
 AC(102)=0.0001  
 AC(104)=0.316  
 AC(106)=117.35  
 AC(107)=0.294  
 AC(110)=1.0E-6  
 AC(111)=0.903  
 AC(112)=1.0  
 AC(113)=1.0  
 AC(114)=0.361  
 AC(118)=1.0E-6  
 AC(120)=1.0E-6  
 AC(121)=1.0E-6

DATA0081  
 DATA0082  
 DATA0083  
 DATA0084  
 DATA0085  
 DATA0086  
 DATA0087  
 DATA0088  
 DATA0089  
 DATA0090  
 DATA0091  
 DATA0092  
 DATA0093  
 DATA0094  
 DATA0095  
 DATA0096  
 DATA0097  
 DATA0098  
 DATA0099  
 DATA0100  
 DATA0101  
 DATA0102  
 DATA0103  
 DATA0104  
 DATA0105  
 DATA0106  
 DATA0107  
 DATA0108  
 DATA0109  
 DATA0110  
 DATA0111  
 DATA0112  
 DATA0113  
 DATA0114  
 DATA0115  
 DATA0116  
 DATA0117  
 DATA0118  
 DATA0119  
 DATA0120

```

C
C
AC(123)=1.0E-6
AC(125)=1.0E-6
AC(127)=1.0E-6
C
C
C      INITIALIZE THE WEIGHTS.
C      DO 6 I=1,KW
C      6 W(I)=0.0
C
C      RETURN
C      END

```

```

DATA0121
DATA0122
DATA0123
DATA0124
DATA0125
DATA0126
DATA0127
DATA0128
DATA0129
DATA0130

```

#### Subroutine INPUT

As in the original subroutine the design data and the coefficients and exponents for the weight equations are read with a namelist statement. The non-zero weight coefficients and exponents are then printed. The major change is that all of the design data is printed in tabular form to facilitate checking.





```

3      DATA CRY//      (C(40),WTOIN ),(C(41),XINLET),(C(42),XLF      )
      ENG//      TUR      ,STOR      ,ABLE      ,      C      ,RYOG      ,ENIC      /,
1      ,      BORA      ,MJET      ,      ,      RA      ,MJET      ,
2      ,      RO      ,CKET      /,
3      SHAPE//      BOO      ,STER      ,TYP      ,E      (N      ,O      WI      ,NGS      ,OR      T      ,AIL      ),
4      ,      ,      ,      ,      ,      ,      ,      ,      ,AIRC      ,RAFT      ,
5      ,      ,      ,      ,      ,      ,      ,      ,      ,LIFT      ,ING      ,BODY      ,
6      ,      ,      ,      ,      ,      ,LI      ,FTIN      ,G      BO      ,DY      P      ,LUS      ,WING      /
      DATA MAX/52/
      NAMELIST /INWAP/ICRY      ,IENG      ,ISHAPE,ACTR      ,AICAPT,ARATIO,CREW      ,
1      ,DM      ,ELBODY,ELNLET,ELRAMP,ENGINS,FCIMOK,GEOFACT,
2      GSPAN      ,HBODY      ,OF      ,OFACS      ,PCHAM      ,PHIGH      ,PLOW      ,QMAX      ,
3      SBODY      ,SFAIR      ,SFUTK      ,SHGRZ      ,SOXTK      ,STPS      ,STSPAN,SVERT      ,
4      SWING      ,TANKS      ,THRUST,TROOT      ,TYTAIL,VFUTK      ,VOXTK      ,WAREF      ,
5      WLANDI,WPAYLO,WPMAIN,WTCIN      ,XINLET,XLF      ,AC
      READ AND PRINT THE NAMELIST VARIABLES.
      READ (NR,INWAP)
      WRITE(NH,INWAP)
      PRINT THE NON-ZERO WEIGHT COEFFICIENTS AND EXPONENTS.
      WRITE(NW,1000)
      LINE=0
      DO 2 I=1,KAC
      IF(AC(I).EQ.0.0) GO TO 2
      WRITE(NW,1002) I,AC(I)
      LINE=LINE+1
      IF(LINE.LT.MAX) GO TO 2
      WRITE(NW,1000)
      LINE=0
2      CONTINUE
      PRINT THE DESIGN DATA.
      WRITE(NW,1004)
      WRITE(NW,1006) SBODY
      WRITE(NW,1008) SFUTK
      WRITE(NW,1010) SOXTK
      WRITE(NW,1012)
      WRITE(NW,1014) SWING
      WRITE(NW,1016) SVERT
INPUT041
INPUT042
INPUT043
INPUT044
INPUT045
INPUT046
INPUT047
INPUT048
INPUT049
INPUT050
INPUT051
INPUT052
INPUT053
INPUT054
INPUT055
INPUT056
INPUT057
INPUT058
INPUT059
INPUT060
INPUT061
INPUT062
INPUT063
INPUT064
INPUT065
INPUT066
INPUT067
INPUT068
INPUT069
INPUT070
INPUT071
INPUT072
INPUT073
INPUT074
INPUT075
INPUT076
INPUT077
INPUT078
INPUT079
INPUT080

```

WRITE(NW,1018) SHORZ  
 WRITE(NW,1020) SFAIR  
 WRITE(NW,1022) STPS  
 WRITE(NW,1024)  
 WRITE(NW,1026) GSPAN  
 WRITE(NW,1028) STSPAN  
 WRITE(NW,1030) TRDQT  
 WRITE(NW,1032) AICAPT  
 WRITE(NW,1034) ARATIO  
 WRITE(NW,1036) ELNLET  
 WRITE(NW,1038) ELRAMP  
 WRITE(NW,1040) ELBODY  
 WRITE(NW,1042) HBCDY  
 WRITE(NW,1044) VFUTK  
 WRITE(NW,1046) VOXTK  
 WRITE(NW,1048)  
 WRITE(NW,1050) (ENG(I,IENG),I=1,3)  
 WRITE(NW,1052) ENGIN  
 WRITE(NW,1054) THRUST  
 WRITE(NW,1056) ACTR  
 WRITE(NW,1058) XINLET  
 WRITE(NW,1060) WAREF  
 WRITE(NW,1062) PCHAM  
 WRITE(NW,1064) PHIGH  
 WRITE(NW,1066) PLOW  
 WRITE(NW,1068)  
 WRITE(NW,1070) WPAYLD  
 WRITE(NW,1072) WPMAN  
 WRITE(NW,1074) WTOIN  
 WRITE(NW,1076) WLANDI  
 WRITE(NW,1078)  
 WRITE(NW,1080) CREW  
 WRITE(NW,1082) OH  
 WRITE(NW,1084) DM  
 WRITE(NW,1086) FCTMCK  
 WRITE(NW,1088) GEDECT  
 WRITE(NW,1090) OF  
 WRITE(NW,1092) OFACS  
 WRITE(NW,1094) QMAX  
 WRITE(NW,1096) TANKS

INPUT081  
 INPUT082  
 INPUT083  
 INPUT084  
 INPUT085  
 INPUT086  
 INPUT087  
 INPUT088  
 INPUT089  
 INPUT090  
 INPUT091  
 INPUT092  
 INPUT093  
 INPUT094  
 INPUT095  
 INPUT096  
 INPUT097  
 INPUT098  
 INPUT099  
 INPUT100  
 INPUT101  
 INPUT102  
 INPUT103  
 INPUT104  
 INPUT105  
 INPUT106  
 INPUT107  
 INPUT108  
 INPUT109  
 INPUT110  
 INPUT111  
 INPUT112  
 INPUT113  
 INPUT114  
 INPUT115  
 INPUT116  
 INPUT117  
 INPUT118  
 INPUT119  
 INPUT120



```

1066 FORMAT(' ',T20,'TURBORAMJET INLET PRESSURE (LOWEK)', ,T57,F9.2)
1068 FORMAT('0',I16,'WEIGHTS')
1070 FORMAT('0',T20,'PAYLOAD',
1072 FORMAT(' ',T20,'MAIN IMPULSE PROPELLANT',
1074 FORMAT(' ',T20,'ESTIMATED TAKEOFF WEIGHT',
1076 FORMAT(' ',T20,'ESTIMATED LANDING WEIGHT',
1078 FORMAT('1',T20,'DESI G N D A T A',/
      1  '0',I16,'OTHER DESIGN DATA')
1080 FORMAT('0',T20,'NUMBER OF CREW',
1082 FORMAT(' ',T20,'DESIGN ALTITUDE',
1084 FORMAT(' ',T20,'DESIGN MACH NUMBER',
1086 FORMAT(' ',T20,'MACH NUMBER FACTOR',
1088 FORMAT(' ',T20,'GEOMETRICAL OUT CF ROUND FACTOR',
1090 FORMAT(' ',T20,'OXIDIZER TO FUEL MIXTURE RATIO',
1092 FORMAT(' ',T20,'ACS OXIDIZER TO FUEL MIXTURE RATIO',
1094 FORMAT(' ',T20,'MAXIMUM DYNAMIC PRESSURE',
1096 FORMAT(' ',T20,'NUMBER OF FUSELAGE FUEL TANKS',
1098 FORMAT(' ',T20,'TAIL TYPE COEFFICIENT',
1100 FORMAT(' ',T20,'ULTIMATE LOAD FACTOR',
1102 FORMAT(' ',T20,'PROPELLANT TYPE',
1104 FORMAT(' ',T20,'SHAPE',
      C
      RETURN
      END
INPUT161
INPUT162
INPUT163
INPUT164
INPUT165
INPUT166
INPUT167
INPUT168
INPUT169
INPUT170
INPUT171
INPUT172
INPUT173
INPUT174
INPUT175
INPUT176
INPUT177
INPUT178
INPUT179
INPUT180
INPUT181
INPUT182
INPUT183
INPUT184

```

### Subroutine MASS

This subroutine has been completely reorganized. With a few exceptions, the component weights that do not depend on the Take-off, Landing or Entry weight have been taken out of the iteration loop. A flow chart of the subroutine developed directly from the coding is shown following the subroutine listing.

The program has a shape flag, ISHAPE, for specifying the vehicle configuration:

ISHAPE = 1    Booster Type (no wings or tail)  
ISHAPE = 2    Aircraft  
ISHAPE = 3    Lifting Body  
ISHAPE = 4    Lifting Body plus Wing

A study of the flow chart shows that there are only two paths through the program; i.e., ISHAPE = 1 and 3 are the same configuration, as are ISHAPE = 2 and 4. Therefore, the Input Data Forms provide only for ISHAPE = 1 and 2.

```

SUBROUTINE MASS
.....
PURPOSE
  CALCULATE THE MASS PROPERTIES AND ITERATE ON THE TAKEOFF
  WEIGHT.
USAGE
  CALL MASS
REMARKS
  THE INPUT AND OUTPUT IS THROUGH THE COMMON BLOCKS.
SUBPRCGRAMS REQUIRED
  ATMOS
.....
  SPECIFICATION STATEMENTS.
COMMON /INOUT/ NR,NW
COMMON /INTGR/ IC(3)
COMMON /CCMON/ C(42)
COMMON /ACOE/ AC(134)
COMMON /WAITS/ W(74)
COMMON /ATMOUT/TE,THETA,DELTA,PE,RHOE,GE,CSE,AMUE
EQUIVALENCE (IC(1),ICRY),(IC(2),IENG),(IC(3),ISHAPE),
EQUIVALENCE (C(1),ACTR),(C(2),AICAPT),(C(3),ARATIO),
EQUIVALENCE (C(4),CREW),(C(5),DH),(C(6),DM),
EQUIVALENCE (C(7),ELBCDY),(C(8),ELNLET),(C(9),ELRAMP),
EQUIVALENCE (C(10),ENGIN),(C(11),FCTMOK),(C(12),GEOFCT),
EQUIVALENCE (C(13),GSPAN),(C(14),HBODY),(C(15),OF),
EQUIVALENCE (C(16),OFACS),(C(17),PCHAM),(C(18),PHIGH),
EQUIVALENCE (C(19),PLOW),(C(20),QMAX),(C(21),SBODY),
EQUIVALENCE (C(22),SFAIR),(C(23),SFUTK),(C(24),SHORZ),
EQUIVALENCE (C(25),SOXTK),(C(26),STPS),(C(27),STSPAN),
EQUIVALENCE (C(28),SVERT),(C(29),SWING),(C(30),TANKS),
EQUIVALENCE (C(31),THRUST),(C(32),TROOT),(C(33),TYTAIL),
EQUIVALENCE (C(34),VFUT),(C(35),VOXTK),(C(36),WAREF),
EQUIVALENCE (C(37),WLANDI),(C(38),WPAYLD),(C(39),WPMANI),
EQUIVALENCE (C(40),WTOIN),(C(41),XINLET),(C(42),XLF),
EQUIVALENCE (W(1),WACS),(W(2),WACSFU),(W(3),WACSOX),

```

```

MASS0001
MASS0002
MASS0003
MASS0004
MASS0005
MASS0006
MASS0007
MASS0008
MASS0009
MASS0010
MASS0011
MASS0012
MASS0013
MASS0014
MASS0015
MASS0016
MASS0017
MASS0018
MASS0019
MASS0020
MASS0021
MASS0022
MASS0023
MASS0024
MASS0025
MASS0026
MASS0027
MASS0028
MASS0029
MASS0030
MASS0031
MASS0032
MASS0033
MASS0034
MASS0035
MASS0036
MASS0037
MASS0038
MASS0039
MASS0040

```

```

C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C
C

```

```

1      (W( 4),WACSP ),(W( 5),WACSRE),(W( 6),WACSTK),
2      (W( 7),WAERO ),(W( 8),WAVONC),(W( 9),WBASIC),
3      (W(10),WBODY ),(W(11),WBPUMP),(W(12),WCONT ),
4      (W(13),WCOVER),(W(14),WCPROV),(W(15),WCREW ),
5      (W(16),WDIST1),(W(17),WDIST2),(W(18),WDRANS),
6      (W(19),WDRY ),(W(20),WELECT),(W(21),WENGMT),
7      (W(22),WENG ),(W(23),WEMPTY),(W(24),WENTRY),
8      (W(25),WFAIR ),(W(26),WFCONT),(W(27),WFRESV),
9      (W(28),WFRAP),(W(29),WFUEL ),(W(30),WFUELM),
      EQUIVALENCE
1      (W(31),WFUNCT),(W(32),WFUSYS),(W(33),WFUTOT),
2      (W(34),WGEAR ),(W(35),WGIMBL),(W(36),WHORZ ),
3      (W(37),WHYPNU),(W(38),WIDUCT),(W(39),WINFUT),
4      (W(40),WINOXT),(W(41),WINSUL),(W(42),WINLET),
5      (W(43),WINSFT),(W(44),WINSOT),(W(45),WLANCH),
6      (W(46),WLAND ),(W(47),WLG ),(W(48),WORESV),
7      (W(49),WORT ),(W(50),WOTRAP),(W(51),WOXCNT),
8      (W(52),WOXID ),(W(53),WOXIDM),(W(54),WOXSYS),
9      (W(55),WOXTOT),(W(56),WP ),(W(57),WPLOSS),
      EQUIVALENCE
1      (W(58),WPRESV),(W(59),WPROPU),(W(60),WPRSYS),
2      (W(61),WPRSYS),(W(62),WREFUL),(W(63),WRESID),
3      (W(64),WSEAL ),(W(65),WSECT),(W(66),WSEP ),
4      (W(67),WSPIKE),(W(68),WSURF ),(W(69),WTHRST),
5      (W(70),WTO ),(W(71),WTPS ),(W(72),WVERT ),
6      (W(73),WVRAMP),(W(74),WING )
      DATA C13,C23,PT2/0.3323333,0.6666667,3000.0/

      INITIALIZE THE TAKEOFF, LANDING AND REENTRY WEIGHTS.
      WTO=WTOIN
      WLAND=WLANDI
      WENTRY=WLAND

      TOTAL THRUST.
      TTOT=THRUST*ENGINES*ACTR

      BODY STRUCTURE.
      WBASIC=AC(14)*SBODY+AC(15)*((ELBODY**XLF/HBODY)**0.15*QMAX**0.16
1      *SBCDY**1.05)**AC(81)+AC(16)
      WSECT=AC(17)*SBODY+AC(18)
      WTHRST=AC(19)*TTOI+AC(20)
      WINFUT=AC(130)*VFUTK+AC(131)

```

MASS0041  
 MASS0042  
 MASS0043  
 MASS0044  
 MASS0045  
 MASS0046  
 MASS0047  
 MASS0048  
 MASS0049  
 MASS0050  
 MASS0051  
 MASS0052  
 MASS0053  
 MASS0054  
 MASS0055  
 MASS0056  
 MASS0057  
 MASS0058  
 MASS0059  
 MASS0060  
 MASS0061  
 MASS0062  
 MASS0063  
 MASS0064  
 MASS0065  
 MASS0066  
 MASS0067  
 MASS0068  
 MASS0069  
 MASS0070  
 MASS0071  
 MASS0072  
 MASS0073  
 MASS0074  
 MASS0075  
 MASS0076  
 MASS0077  
 MASS0078  
 MASS0079  
 MASS0080

```

C
C
WINOXT=AC(132)*VOXTK+AC(133)
WBODY=WASIC+WSECT+WTHRST+WINFUT+WINOXT

C
C
THERMAL PROTECTION SYSTEM.
WINSUL=AC(21)*STPS+AC(76)
WCOVER=AC(22)*STPS+AC(77)
WTPS=WINSUL+WCOVER

C
C
MAIN PROPULSION SYSTEM.
GO TO(10,20,30),IENG

C
C
TURBORAMJET ENGINE.
10 CALL ATMDS(DH,IERR)
X=1.0+0.2*DM**2
PTO=PE*X**3*SQRT(X)
PR=1.0
IF(DM.LE.1.0) GO TO 14
IF(DM.GT.5.0) GO TO 12
PR=1.0-0.076*(DM-1.0)**1.35
GO TO 14
12 PR=800.0/(DM**4+935.0)
14 PT2=PR*PTO/144.0
WA=WAREF*ACTR
WENG=(AC(32)*EXP(AC(33)*WA)*((PT2-PHIGH)/(PLOW-PHIGH))
+AC(34)*EXP(AC(35)*WA)*((PT2-PLOW)/(PHIGH-PLOW)))*ENGIN
1
2
GO TO (50,40),ICRY

C
C
RAMJET ENGINE.
20 WENG=AC(82)*TTOT+AC(83)
GO TO (50,40),ICRY

C
C
ROCKET ENGINE.
30 WENG=AC(28)*TTOT+AC(29)*TTOT*ARATIO**AC(30)+AC(31)*ENGIN
WGIMBL=AC(55)*(750.0*(TTOT/ENGIN/PCHAM)**1.25)**AC(110)+AC(56)

C
C
CRYOGENIC FUEL SYSTEMS.
40 WFUNCT=AC(36)*VFUTK+AC(37)
WOXCNT=AC(38)*VOXTK+AC(39)
WINSFT=AC(40)*SFUTK+AC(41)

```

MASS0081  
 MASS0082  
 MASS0083  
 MASS0084  
 MASS0085  
 MASS0086  
 MASS0087  
 MASS0088  
 MASS0089  
 MASS0090  
 MASS0091  
 MASS0092  
 MASS0093  
 MASS0094  
 MASS0095  
 MASS0096  
 MASS0097  
 MASS0098  
 MASS0099  
 MASS0100  
 MASS0101  
 MASS0102  
 MASS0103  
 MASS0104  
 MASS0105  
 MASS0106  
 MASS0107  
 MASS0108  
 MASS0109  
 MASS0110  
 MASS0111  
 MASS0112  
 MASS0113  
 MASS0114  
 MASS0115  
 MASS0116  
 MASS0117  
 MASS0118  
 MASS0119  
 MASS0120





```

      WPRESV=WFRESV+WRESV
      WPLOSS=AC(116)*WPMAIN
      WFUEL=WFUELM+WFRESV
      WOXID=WOXIDM+WRESV
      WFTRAP=AC(92)*WFUEL+AC(93)
      WOTRAP=AC(94)*WOXID+AC(95)
      WFUTOT=WFUEL+WFTRAP
      WOXTOT=WOXID+WOTRAP
      WP=WFUTOT+WOXTOT
      WRESID=WFTRAP+WOTRAP
      C
      C
      CREW.
      WCREW=AC(72)*CREW+AC(73)
      C
      C
      ITERATE ON THE WEIGHTS.
      C
      C
      WRITE(NW,1000)
      NO=0
      70 NO=NO+1
      WTOX=WTO
      C
      C
      AERODYNAMIC SURFACES.
      GO TO(90,80,90,80),ISHAPE
      80 WHING=AC(1)*(WTO*XLF*STSPAN*SWING/TROOT)**AC(78)*1.0E-06
      1   +AC(2)*SWING+AC(3)
      2   +AC(117)*((WLAND*XLF*STSPAN*SWING/TROOT)*1.0E-09)**AC(118)
      WVERT=AC(4)*SVERT**AC(89)+AC(5)
      WHORZ=AC(6)*((WTO/SWING)**0.6*SHORZ**1.2*QMAX**0.8)**AC(90)+AC(7)
      1   +AC(119)*((WLAND/SWING)**0.6*SHORZ**1.2*QMAX**0.8)**AC(120)
      90 WFAIR=AC(8)*SFAIR+AC(9)
      WSURF=WHING+WVERT+WHORZ+WFAIR
      C
      C
      LAUNCH AND RECOVERY SYSTEMS.
      WLAUNCH=AC(23)*WTO+AC(24)
      WLG=AC(25)*WTO**AC(101)+AC(26)*WLAND**AC(121)+AC(27)
      WGEAR=WLAUNCH+WLG
      C
      C
      ORIENTATION AND SEPARATION SYSTEMS.
      WACSFU=AC(96)*WTO+AC(97)+AC(134)*WENTRY
      WACSOX=WACSFU*OFACS
      MASS0161
      MASS0162
      MASS0163
      MASS0164
      MASS0165
      MASS0166
      MASS0167
      MASS0168
      MASS0169
      MASS0170
      MASS0171
      MASS0172
      MASS0173
      MASS0174
      MASS0175
      MASS0176
      MASS0177
      MASS0178
      MASS0179
      MASS0180
      MASS0181
      MASS0182
      MASS0183
      MASS0184
      MASS0185
      MASS0186
      MASS0187
      MASS0188
      MASS0189
      MASS0190
      MASS0191
      MASS0192
      MASS0193
      MASS0194
      MASS0195
      MASS0196
      MASS0197
      MASS0198
      MASS0199
      MASS0200

```

```

C
C
WACSP=WACSFU+WACSOX
WACSRE=AC(115)*WACSP
WACS=AC(57)*WTO+AC(58)+AC(59)+AC(124)*WENTRY**AC(125)
WACSTK=AC(64)*WACSP+AC(65)
WAERO=AC(60)*(WTO**C23*(ELBODY+GSPAN)**0.25)**AC(111)+AC(61)
1 +AC(122)*WENTRY**C23*(ELBODY+GSPAN)**0.25)**AC(123)
WSEP=AC(62)*WTO+AC(63)
WORNT=WGIMBL+WACS+WACSTK+WAERO+WSEP
C
C
POWER SUPPLY.
WELECT=AC(66)*(SQRT(WTO)*ELBODY**0.25)**AC(112)+AC(67)
1 +AC(126)*(SQRT(WENTRY)*ELBODY**0.25)**AC(127)
WHYPNU=AC(68)*((SWTIG+SHORZ+SVERT)*0.0010*QMAX)**0.3340
1 *(SQRT(ELBODY+STSPAN)*TYTAIL)**AC(113)+AC(69)
2 +AC(128)*WTO+AC(129)*WENTRY
WPNRSY=WELECT+WHYPNU
C
C
AVIONICS AND CREW SYSTEMS.
WAVONC=AC(70)*WTO**AC(114)+AC(71)
WCPROV=AC(74)*WTO+AC(80)*CREW+AC(75)
C
C
DRY WEIGHT AND DESIGN RESERVE.
WDRY=WSURF+WBODY+WTPS+WGEAR+WPROPU+WORNT+WPNRSY+WAVONC+WCPROV
WCCNT=AC(58)*WDRY+AC(99)
C
C
EMPTY, LANDING, ENTRY AND TAKEOFF WEIGHTS.
WEMPTY=WDRY+WCONT
WLAND=WEMPTY+WPAYLO+WCREW+WRESID+WACSRE
WENTRY=WLAND+WACSP
WTC=WENTRY+WPHAIN+WPRESV+WPLOSS
C
C
PRINT THE WEIGHTS AND CHECK FOR CONVERGENCE.
WRITE(NH,1002) NO,WDRY,WEMPTY,WLAND,WENTRY,WTO
If (ABS((WTOX-WTO)/WTO).GT.0.001) GO TO 70
C
RETURN
C
C
FORMAT STATEMENTS.
1000 FORMAT('1','0','13','MASS ITERATION'/
1 '0','119','DRY EMPTY LANDING ENTRY',

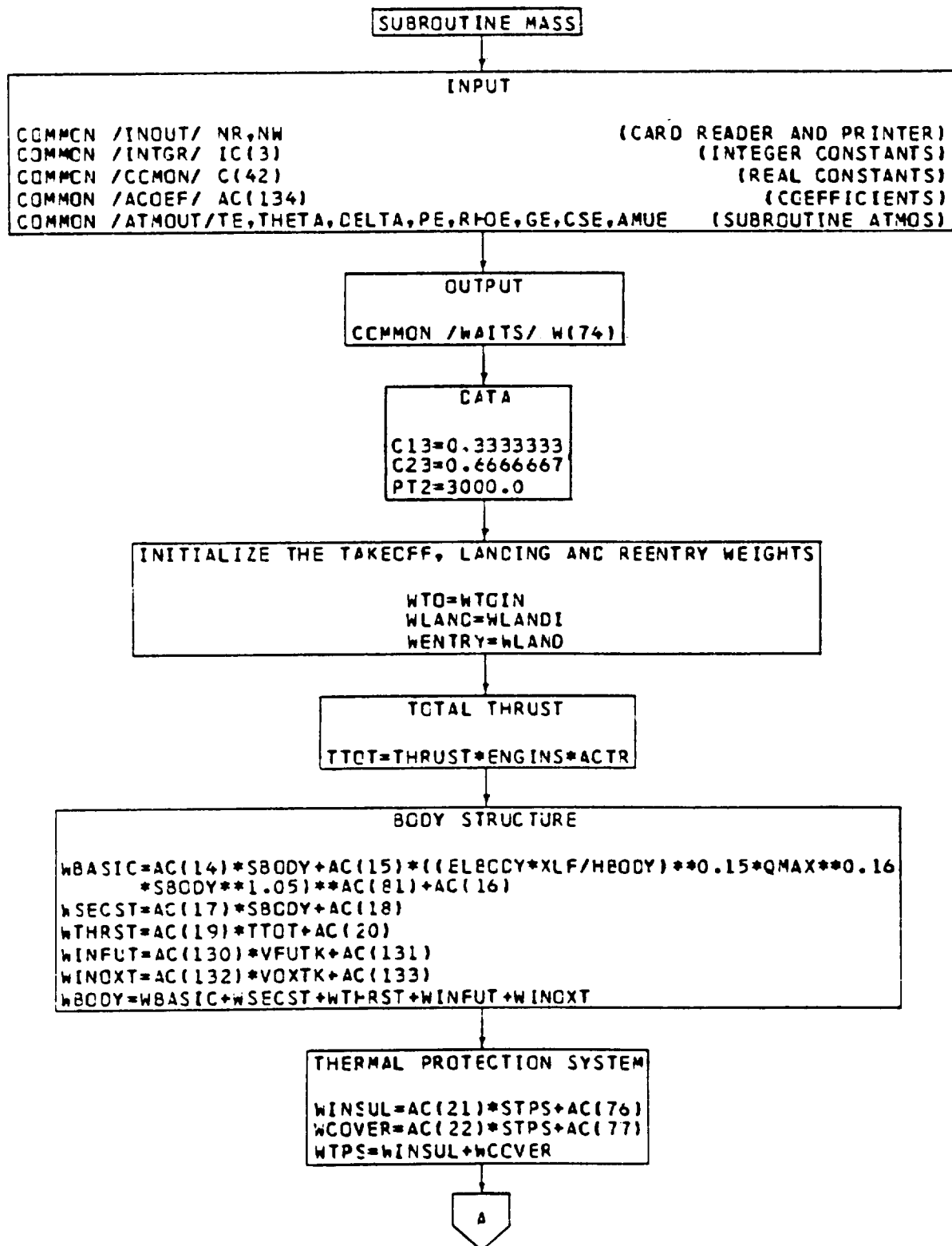
```

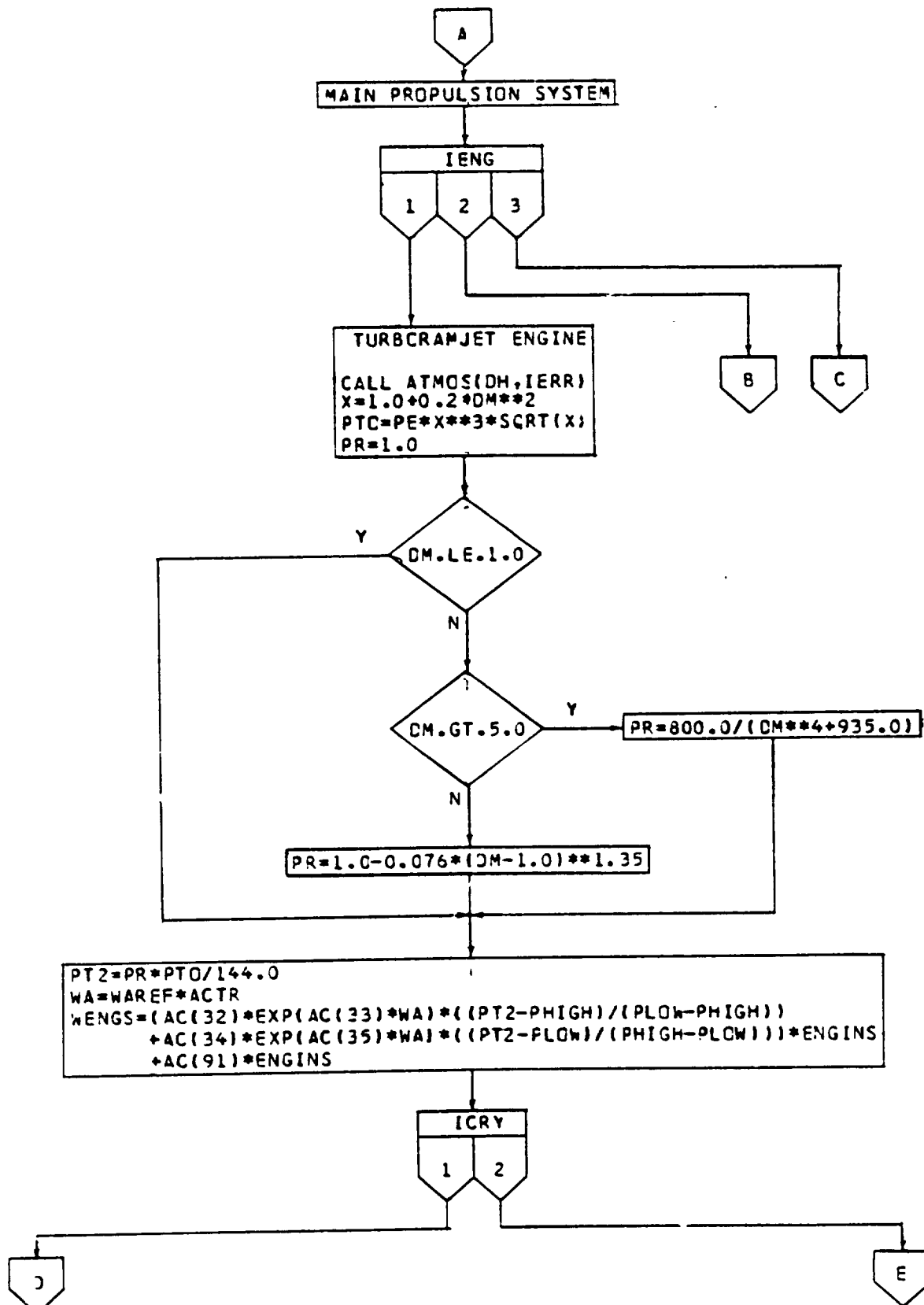
MASS0201  
 MASS0202  
 MASS0203  
 MASS0204  
 MASS0205  
 MASS0206  
 MASS0207  
 MASS0208  
 MASS0209  
 MASS0210  
 MASS0211  
 MASS0212  
 MASS0213  
 MASS0214  
 MASS0215  
 MASS0216  
 MASS0217  
 MASS0218  
 MASS0219  
 MASS0220  
 MASS0221  
 MASS0222  
 MASS0223  
 MASS0224  
 MASS0225  
 MASS0226  
 MASS0227  
 MASS0228  
 MASS0229  
 MASS0230  
 MASS0231  
 MASS0232  
 MASS0233  
 MASS0234  
 MASS0235  
 MASS0236  
 MASS0237  
 MASS0238  
 MASS0239  
 MASS0240

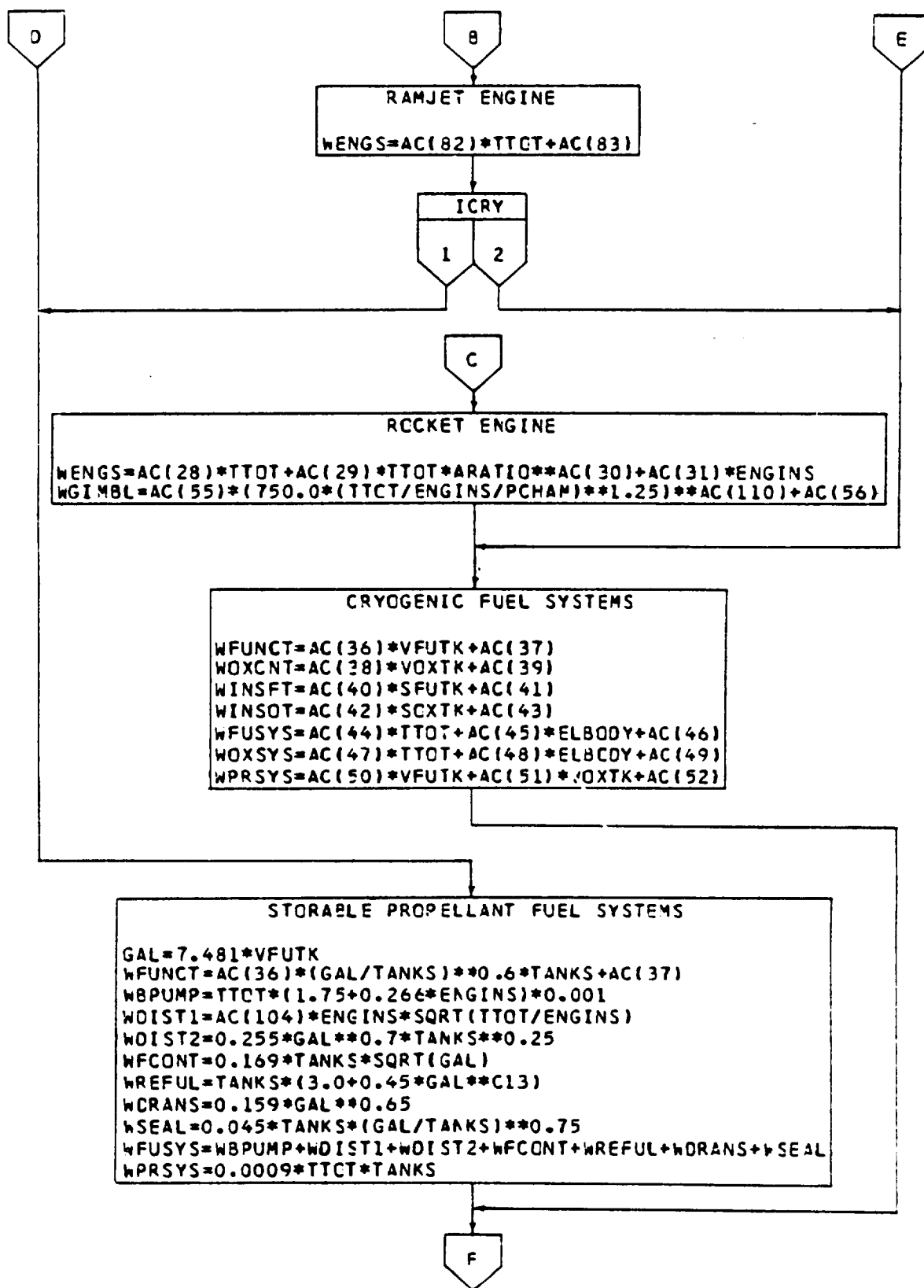
```

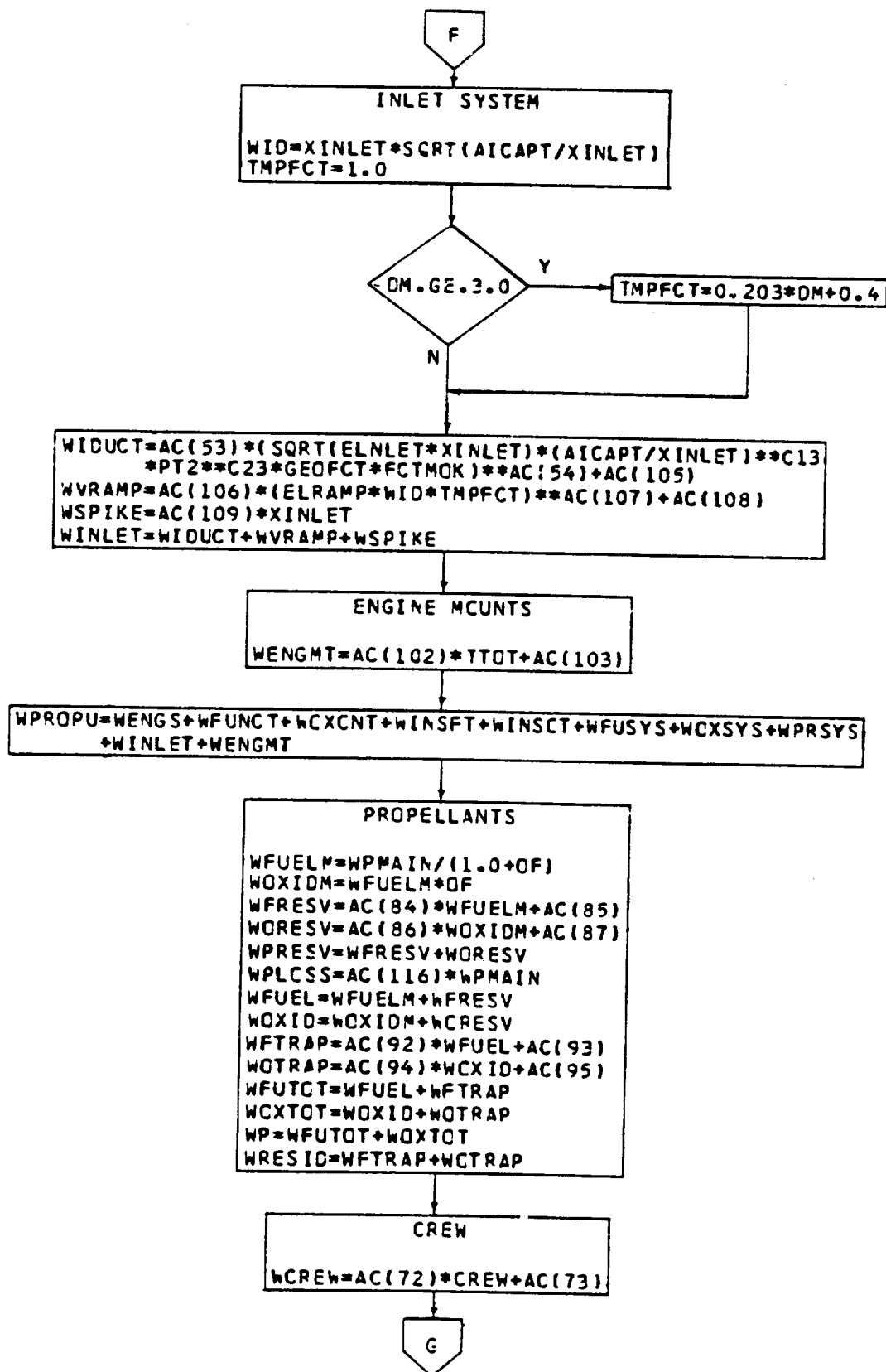
2      T65,'TAKEOFF' /
3      ' ,T11,'NO  WEIGHT
4      ,T66,'WEIGHT' /)
1002 FORMAT( ' ,T11,I2,5F12.0)
      END
      WEIGHT
      WEIGHT
      MASS0241
      MASS0242
      MASS0243
      MASS0244
      MASS0245

```

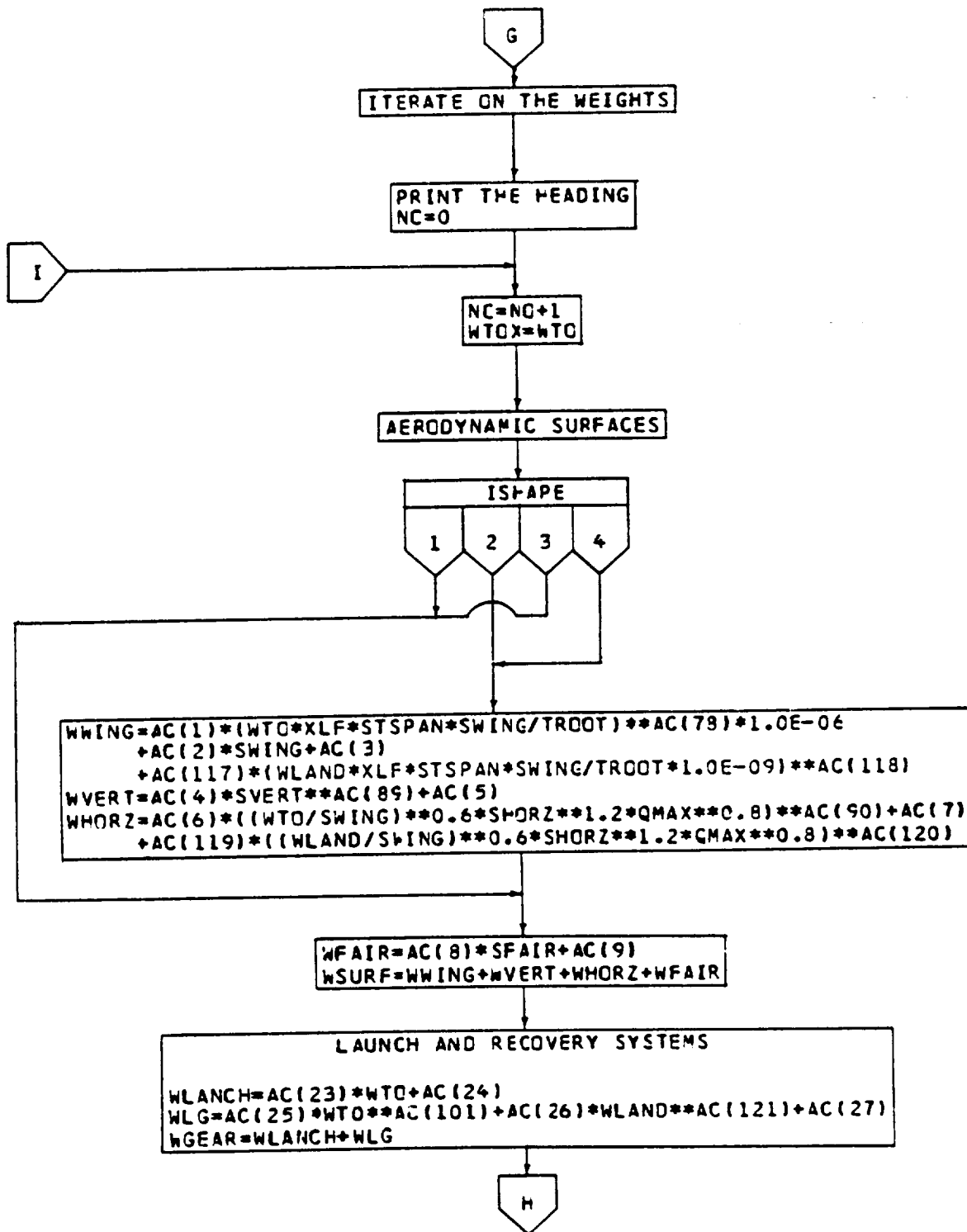


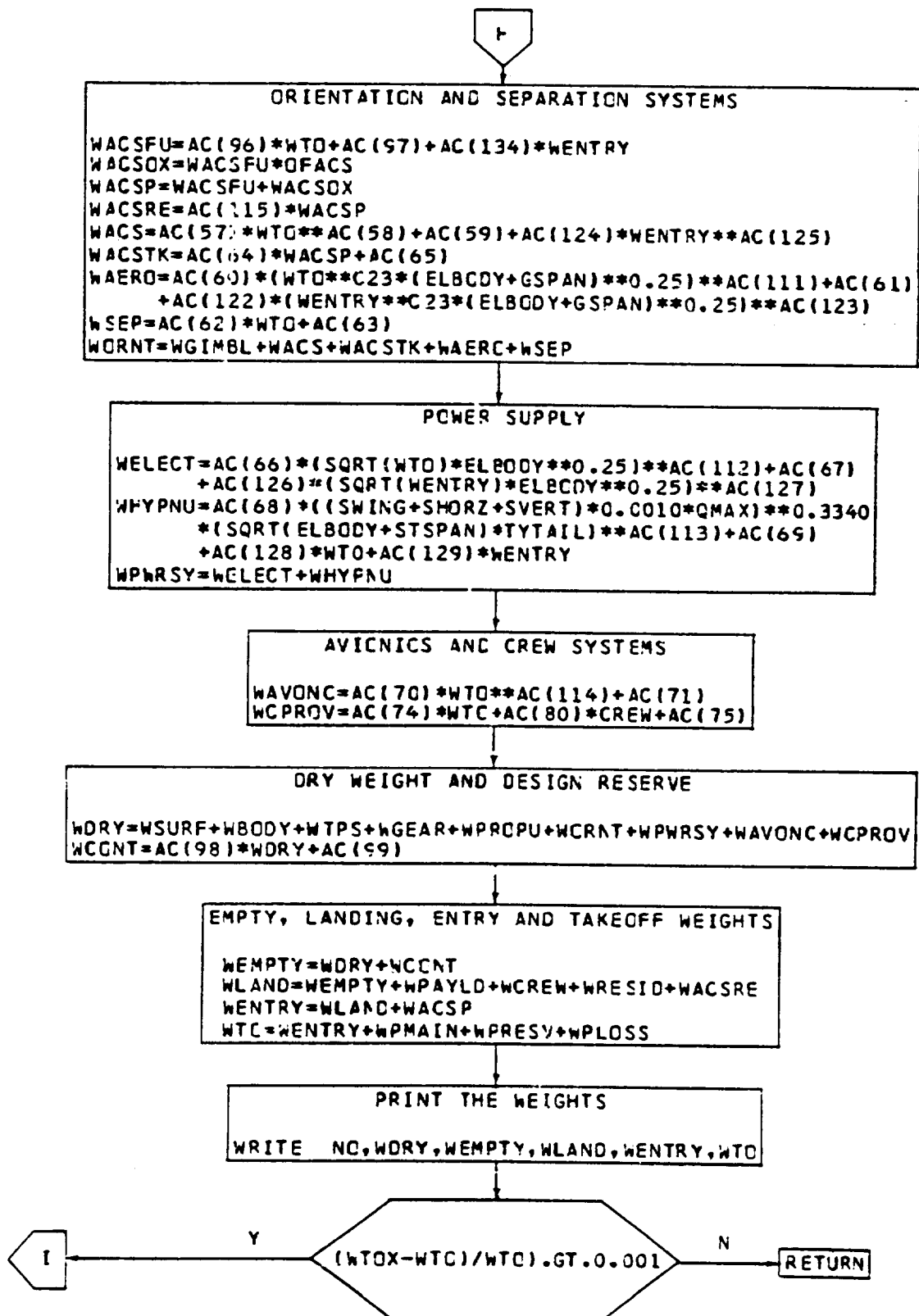












### Subroutine ATMOS

This subroutine has been extensively revised. The input is the geometric altitude (ft). The output, through common block ATMOUT, is the temperature ( $^{\circ}\text{R}$ ), the temperature ratio, the pressure ratio, the pressure (psf), the density (pcf), the gravitational acceleration ( $\text{ft}/\text{sec}^2$ ), the speed of sound ( $\text{ft}/\text{sec}$ ) and the coefficient of viscosity ( $\text{lb}/\text{ft}\text{-sec}$ ). Although the output is all in English units, all internal calculations are in SI units.



```

C      HM=90000. METERS FROM THE EQUATION ROM=HM+ZM/({ZM-HM}).
C
C      REFERENCE
C      *U.S. STANDARD ATMOSPHERE, 1962 (ICAO STANDARD ATMOSPHERE TO 32 KILOMETERS, PROPOSED ICAO EXTENSION TO 700 KILOMETERS AND DATA TO 700 KILOMETERS), PREPARED UNDER SPONSORSHIP OF THE NATIONAL AERONAUTICS AND SPACE ADMINISTRATION, UNITED STATES AIR FORCE AND UNITED STATES WEATHER BUREAU.
C
C      SUBPROGRAMS REQUIRED
C      NCNE
C
C      SPECIFICATION STATEMENTS.
C      COMMON /ATMOUT/TE,THETA,DELTA,PE,RHOE,GE,CSE,AMUE
C      DATA C1,C2/0.0187434,49.0222/
C      DATA GOE,ROM,FTM/32.1741,6354501.0,0.3048/
C      DATA POM,TOM/760.0,288.15/
C
C      SET THE SWITCHES.
C      JSWA=1
C      IERR=0
C
C      CLACULATE THE ALTITUDES IN METERS.
C      ZM=FTM+ZE
C      HM=ROM+ZM/(ROM+ZM)
C
C      SELECT THE ALTITUDE RANGE.
C      IF(HM.LT.0.0) GO TO 26
C      IF(HM.LT.11000.0) GO TO 2
C      IF(HM.LT.20000.0) GO TO 4
C      IF(HM.LT.32000.0) GO TO 6
C      IF(HM.LT.47000.0) GO TO 8
C      IF(HM.LT.52000.0) GO TO 10
C      IF(HM.LT.61000.0) GO TO 12
C      IF(HM.LT.79000.0) GO TO 14
C      IF(HM.LE.90000.0) GO TO 16
C      GO TO 26
C
C      SPECIFY THE ALTITUDE, PRESSURE AND TEMPERATURE AT THE BASE OF
C
C
C      ATMOS041
C      ATMOS042
C      ATMOS043
C      ATMOS044
C      ATMOS045
C      ATMOS046
C      ATMOS047
C      ATMOS048
C      ATMOS049
C      ATMOS050
C      ATMOS051
C      ATMOS052
C      ATMOS053
C      ATMOS054
C      ATMOS055
C      ATMOS056
C      ATMOS057
C      ATMOS058
C      ATMOS059
C      ATMOS060
C      ATMOS061
C      ATMOS062
C      ATMOS063
C      ATMOS064
C      ATMOS065
C      ATMOS066
C      ATMOS067
C      ATMOS068
C      ATMOS069
C      ATMOS070
C      ATMOS071
C      ATMOS072
C      ATMOS073
C      ATMOS074
C      ATMOS075
C      ATMOS076
C      ATMOS077
C      ATMOS078
C      ATMOS079
C      ATMOS080

```

C THE LAYER AND THE TEMPERATURE GRADIENT.

```

2 HBM=0.0
  PBM=760.0
  TBM=288.15
  ALM=-0.0065
  GO TO 18

4 HBM=11000.0
  PBM=169.754
  TBM=216.65
  ALM=0.0
  JSWA=2
  GO TO 18

6 HBM=20000.0
  PBM=41.0649
  TBM=216.65
  ALM=0.001
  GO TO 18

8 HBM=32000.0
  PBM=6.51064
  TBM=228.65
  ALM=0.0028
  GO TO 18

10 HBM=47000.0
  PBM=0.831859
  TBM=270.65
  ALM=0.0
  JSWA=2
  GO TO 18

12 HBM=52000.0
  PBM=0.44254
  TBM=270.65
  ALM=-0.002
  GO TO 18

14 HBM=61000.0
  PBM=0.136585
  TBM=252.65
  ALM=-0.004
  GO TO 18

16 HBM=79000.0
  PBM=0.0077834

```

ATMOS081  
 ATMOS082  
 ATMOS083  
 ATMOS084  
 ATMC085  
 ATMOS086  
 ATMC087  
 ATMOS088  
 ATMC089  
 ATMOS090  
 ATMC091  
 ATMOS092  
 ATMC093  
 ATMOS094  
 ATMC095  
 ATMOS096  
 ATMC097  
 ATMOS098  
 ATMC099  
 ATMOS100  
 ATMC101  
 ATMOS102  
 ATMC103  
 ATMOS104  
 ATMC105  
 ATMOS106  
 ATMC107  
 ATMOS108  
 ATMC109  
 ATMOS110  
 ATMC111  
 ATMOS112  
 ATMC113  
 ATMOS114  
 ATMC115  
 ATMOS116  
 ATMC117  
 ATMOS118  
 ATMC119  
 ATMOS120



### Subroutine PRINT

The only modifications to this subroutine were format changes to improve the readability of the Weight Statement.



C	SUBROUTINE PRINT	PRINT001
C	.....	PRINT002
C		PRINT003
C	PURPOSE	PRINT004
C	PRINT THE AIRCRAFT WEIGHT STATEMENT.	PRINT005
C		PRINT006
C	USAGE	PRINT007
C	CALL PRINT	PRINT008
C		PRINT009
C	REMARKS	PRINT010
C	THE WEIGHTS ARE BROUGHT IN THROUGH THE COMMON BLOCKS /COMMON/PRINT011	
C	AND /WAITS/.	PRINT012
C		PRINT013
C	SUBPROGRAMS REQUIRED	PRINT014
C	NONE	PRINT015
C	.....	PRINT016
C		PRINT017
C	SPECIFICATION STATEMENTS.	PRINT018
	COMMON /INOUT/ NR,NW	PRINT019
	COMMON /COMMON/ C(42)	PRINT020
	COMMON /WAITS/ W(74)	PRINT021
	EQUIVALENCE (C(38),WPAYLD),(C(39),WPMAIN)	PRINT022
1	EQUIVALENCE (W( 1),WACS ),(W( 2),WACSFU),(W( 3),WACSOX),	PRINT023
2	(W( 4),WACSP ),(W( 5),WACSRE),(W( 6),WACSTK),	PRINT024
3	(W( 7),WAERO ),(W( 8),WAVONG),(W( 9),WEASIC),	PRINT025
4	(W(10),WBODY ),(W(11),WBUMP),(W(12),WCONT ),	PRINT026
5	(W(13),WCOVER),(W(14),WCPROV),(W(15),WCREW ),	PRINT027
6	(W(16),WDIST1),(W(17),WDIST2),(W(18),WDRANS),	PRINT028
7	(W(19),WDRY ),(W(20),WELECT),(W(21),WENGMT),	PRINT029
8	(W(22),WENG ),(W(23),WEMPTY),(W(24),WENTRY),	PRINT030
9	(W(25),WFAIR ),(W(26),WFCONT),(W(27),WFRESV),	PRINT031
	(W(28),WTRAP),(W(29),WFUEL ),(W(30),WFUELM)	PRINT032
	EQUIVALENCE (W(31),WFUNCT),(W(32),WFUSYS),(W(33),WFUTOT),	PRINT033
1	(W(34),WGEAR ),(W(35),WGIMBL),(W(36),WHORZ ),	PRINT034
2	(W(37),WHYPNU),(W(38),WIDUCT),(W(39),WINFUT),	PRINT035
3	(W(40),WINOXT),(W(41),WINSUL),(W(42),WINLET),	PRINT036
4	(W(43),WINSFT),(W(44),WINSOT),(W(45),WLANCH),	PRINT037
5	(W(46),WLAND ),(W(47),WLS ),(W(48),WORESV),	PRINT038
6	(W(49),WORNT ),(W(50),WOTRAP),(W(51),WOXCNT),	PRINT039
7	(W(52),WOXID ),(W(53),WOXIDM),(W(54),WOXSYS),	PRINT040

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8      (W(55),WOXTOT),(W(56),WP      ),(W(57),WPLOSS),
9      (W(58),WPRESV),(W(59),MPROP), (W(60),WPRSYS)
EQUIVALENCE (W(61),WPRSYS),(W(62),WREFUL),(W(63),WRESID),
1      (W(64),WSEAL ),(W(65),WSECS),(W(66),WSEP ),
2      (W(67),WSPIKE),(W(68),WSURF ),(W(69),WTHRST),
3      (W(70),WTO ),(W(71),WTPS ),(W(72),WVERT ),
4      (W(73),WVRAMP),(W(74),WHING )

C      PRINT THE WEIGHTS.
C      WRITE(NW,1000)
WRITE(NW,1002) WSURF,WHING,WVERT,WHORZ,WFAIR
WRITE(NW,1004) WBODY,WBASIC,WSECS,WTHRST,WINFUT,WINOXT
WRITE(NW,1006) WTPS,WINSUL,WCOVER
WRITE(NW,1008) WGEAR,WLANCH,WLG
WRITE(NW,1010) WPROP,WENG,WENGMT,WFUNCT,WOXCNT,WINSFT,WINSOT,
1      WUSYS,WOXSYS,WPRSYS,WINLET
WRITE(NW,1012) WCRNT,WGIMBL,WACS,WACSTK,WAERO,WSEP
WRITE(NW,1014) WPRSYS,WELCT,WHYPNU
WRITE(NW,1016) WAVONC
WRITE(NW,1018) WCPROV
WRITE(NW,1020) WDRY
WRITE(NW,1000)
WRITE(NW,1020) WDRY
WRITE(NW,1022) WCONT
WRITE(NW,1024) WEMPTY
WRITE(NW,1026) WPAYLD
WRITE(NW,1028) WCREW
WRITE(NW,1030) WRESID,WFTAP,WOTRAP
WRITE(NW,1032) WLAND
WRITE(NW,1034) WACSP,WACSFU,WACSOX
WRITE(NW,1036) WENTRY
WRITE(NW,1038) WPMIN,WFUERM,WOXIDM
WRITE(NW,1040) WPRESV,WFRESV,WORESV
WRITE(NW,1042) WPLOSS
WRITE(NW,1044) WTD

C      RETURN
C      FORMAT STATEMENTS.
C      1000 FORMAT('1.//0',T30,'W E I G H T S T A T E M E N T')
PRINT041
PRINT042
PRINT043
PRINT044
PRINT045
PRINT046
PRINT047
PRINT048
PRINT049
PRINT050
PRINT051
PRINT052
PRINT053
PRINT054
PRINT055
PRINT056
PRINT057
PRINT058
PRINT059
PRINT060
PRINT061
PRINT062
PRINT063
PRINT064
PRINT065
PRINT066
PRINT067
PRINT068
PRINT069
PRINT070
PRINT071
PRINT072
PRINT073
PRINT074
PRINT075
PRINT076
PRINT077
PRINT078
PRINT079
PRINT080

```



```

1022 FORMAT('0',T13,'DESIGN RESERVE'
1024 FORMAT('0',T11,'EMPTY WEIGHT'
1026 FORMAT('0',T13,'PAYLOAD'
1028 FORMAT('0',T13,'CREW'
1030 FORMAT('0',T13,'RESIDUAL PROPELLANTS'
      1  ' ',T15,'TRAPPED FUEL'
      2  ' ',T15,'TRAPPED OXIDIZER'
1032 FORMAT('0',T11,'LANDING WEIGHT'
1034 FORMAT('0',T13,'ATTITUDE CONTROL SYSTEM PROPELLANTS'
      1  ' ',T15,'FUEL'
      2  ' ',T15,'OXIDIZER'
1036 FORMAT('0',T11,'ENTRY WEIGHT'
1038 FORMAT('0',T13,'MAIN PROPELLANTS'
      1  ' ',T15,'FUEL'
      2  ' ',T15,'OXIDIZER'
1040 FORMAT('0',T13,'RESERVE PROPELLANTS'
      1  ' ',T15,'FUEL'
      2  ' ',T15,'OXIDIZER'
1042 FORMAT('0',T13,'INFLIGHT LOSSES'
1044 FORMAT('0',T11,'TAKEOFF WEIGHT'
C
      END
PRINT121
PRINT122
PRINT123
PRINT124
PRINT125
PRINT126
PRINT127
PRINT128
PRINT129
PRINT130
PRINT131
PRINT132
PRINT133
PRINT134
PRINT135
PRINT136
PRINT137
PRINT138
PRINT139
PRINT140
PRINT141
PRINT142

```

## Input Data

The input to the program consists of two types of data-- design data and weight coefficients and exponents. The design data describes the vehicle, while the weight coefficients and exponents define the equations that will be used to calculate the weights. The variable names, the compiled values of the variables and their definitions are tabulated on the following pages. Since the data is read with a NAMELIST Statement, only those values that differ from the compiled values need be input.

Design Data. -- The path through the program is determined by the values of the Integer Design Data: ICRY (Propellant Type), IENG (Engine Type) and ISHAPE (Vehicle Configuration). There are two propellant types (storable and cryogenic) and three engine types (turboramjet, ramjet and rocket). The program also provides for four vehicle configurations:

1. Booster Type (no wings and tail)
2. Aircraft
3. Lifting Body
4. Lifting Body plus Wing

However, the path through the program is the same for shapes 1 and 3, and is the same for shapes 2 and 4. This gives a total of only twelve combinations, which can be reduced to ten by omitting the storable propellant-rocket engine combination. The input data forms discussed in the next section have been prepared for these ten combinations. Note that the compiled values of the Integer Design Data define the same vehicle configuration (cryogenic propellant, rocket engine and aircraft shape) as the original WAATS program, but the Engine Type Indicators have been rearranged. The majority of the Real Design Data is set to zero; however, selected values have been specified to reduce the amount of input data.

Note that the takeoff and landing weights must be estimated. These estimates are only used for the first iteration, so they need not be accurate.

Weight Coefficients and Exponents. -- The most difficult task in preparing the input data is the specification of the Weight Coefficients and Exponents. The input data form in the next section simplifies the task by showing which values must be specified for each vehicle configuration. In addition, the equations of ref. 5 have been studied and values of the coefficients and exponents have been specified, where possible. In cases where ref. 5 gives more than one set of coefficients and exponents for

a component, the values specified are for high speed and/or rocket powered aircraft. Some of the equations have one term with takeoff weight as the parameter and another term with landing or entry weights as the parameter. In these cases, the coefficients and exponents for the takeoff weight term are specified. The exponents not otherwise specified are set to  $1.0E-6$  to eliminate error messages when the program is run on an IBM computer.

# WAATS DESIGN DATA

SYMBOL	COMPILED VALUE	DEFINITION
ICRY	2	PROPELLANT TYPE INDICATOR, ICRY=1 STORABLE. ICRY=2 CRYOGENIC.
IENG	3	ENGINE TYPE INDICATOR, IENG=1 TURBORAMJET. IENG=2 RAMJET. IENG=3 ROCKET.
ISHAPE	2	SHAPE FLAG, ISHAPE=1 BOOSTER TYPE (NO WINGS OR TAIL). ISHAPE=2 AIRCRAFT. ISHAPE=3 LIFTING BODY. ISHAPE=4 LIFTING BODY PLUS WING.
ACTR	1.0	THRUST SCALING FACTOR.
AICAPT	0.0	TOTAL CAPTURE AREA OF INLETS, SQ. FT.
ARATIO	0.0	ROCKET ENGINE AREA RATIO (AIRCRAFT).
CREW	2.0	NUMBER OF CREW MEMBERS.
DH	0.0	DESIGN ALTITUDE, FT.
DM	1.0	DESIGN MACH NUMBER.
ELBCDY	0.0	BCDY REFERENCE LENGTH, FT.
ELNLET	0.0	TOTAL INLET LENGTH, FT.
ELRAMP	0.0	TOTAL RAMP LENGTH, FT.
ENGINS	2.0	NUMBER OF ENGINES.
FCTMCK	1.0	MACH NUMBER FACTOR.
GEOFCT	1.0	GEOMETRICAL OUT OF ROUND FACTOR.
GSPAN	0.0	GEOMETRIC WING SPAN, FT.
HBODY	1.0	MAXIMUM BODY HEIGHT, FT.
OF	6.0	OXIDIZER TO FUEL MIXTURE RATIO BY WEIGHT.
OFACS	0.0	ACS OXIDIZER TO FUEL MIXTURE RATIO BY WEIGHT.
PCHAM	1000.0	ROCKET ENGINE CHAMBER PRESSURE, PSIA.
PHIGH	176.0	TURBORAMJET INLET PRESSURE (UPPER CURVE), PSIA.
PLGW	46.0	TURBORAMJET INLET PRESSURE (LOWER CURVE), PSIA.
QMAX	0.0	MAXIMUM DYNAMIC PRESSURE, LB/SQ. FT.
SBODY	0.0	TOTAL BODY WETTED AREA, SQ. FT.
SFAIR	0.0	TOTAL FAIRING OR ELEVON SURFACE PLANFORM, SQ. FT.
SFUTK	0.0	FUEL TANK WETTED AREA, SQ. FT.
SHORZ	0.0	TOTAL HORIZONTAL SURFACE PLANFORM AREA, SQ. FT.
SOXTK	0.0	OXICIZED TANK WETTED AREA, SQ. FT.
STPS	0.0	THERMAL PROTECTION SYSTEM AREA, SQ. FT.
STSPAN	0.0	WING STRUCTUAL SPAN (ALONG 50 PERCENT CHORD), FT.
SVERT	0.0	TOTAL VERTICAL SURFACE PLANFORM AREA, SQ. FT.
SWING	0.0	THEORETICAL WING AREA, SQ. FT.
TANKS	1.0	NUMBER OF FUSELAGE FUEL TANKS.
THRUST	0.0	THRUST OF ONE ENGINE, LB.
TRCCT	0.0	WING THICKNESS AT THEORETICAL ROOT, FT.
TYTAIL	1.25	TAIL TYPE COEFFICIENT.
VFUTK	0.0	VOLUME OF FUEL TANK, CU. FT.
VOXTK	0.0	VOLUME OF OXICIZER TANK, CU. FT.
WAREF	0.0	REFERENCE ENGINE AIRFLOW, LB/SEC.

# WAATS DESIGN DATA

SYMBOL	COMPILED VALUE	DEFINITION
WLANDI	0.0	ESTIMATED LANDING WEIGHT, LB.
WPAYLO	0.0	WEIGHT OF PAYLOAD, LB.
WPMAIN	0.0	WEIGHT OF MAIN IMPULSE PROPELLANT, LB.
WTOIN	0.0	ESTIMATED TAKEOFF WEIGHT, LB.
XINLET	1.0	NUMBER OF INLETS.
XLF	4.0	WING ULTIMATE LOAD FACTOR.



# WAATS WEIGHT COEFFICIENTS AND EXPONENTS

COEF.	COMPILED VALUE	DEFINITION
AC(1)	2905.0	WING WEIGHT COEFFICIENT.
AC(2)	0.0	WING WEIGHT CCEFFICIENT.
AC(3)	0.0	FIXED WING WEIGHT.
AC(4)	5.0	VERTICAL TAIL WEIGHT COEFFICIENT
AC(5)	0.0	FIXED VERTICAL TAIL WEIGHT.
AC(6)	0.00035	HORIZONTAL TAIL WEIGHT COEFFICIENT.
AC(7)	0.0	FIXED HORIZONTAL TAIL WEIGHT.
AC(8)	0.0	FAIRING WEIGHT COEFFICIENT.
AC(9)	0.0	FIXED FAIRING WEIGHT.
AC(10)		NOT USED.
AC(11)		NOT USED.
AC(12)		NOT USED.
AC(13)		NOT USED.
AC(14)	0.0	BODY WEIGHT COEFFICIENT.
AC(15)	0.341	BODY WEIGHT CCEFFICIENT.
AC(16)	0.0	FIXED BODY WEIGHT.
AC(17)	0.98	SECONDARY STRUCTURE WEIGHT COEFFICIENT.
AC(18)	0.0	FIXED SECONDARY STRUCTURE WEIGHT.
AC(19)	0.0025	THRUST STRUCTURE WEIGHT COEFFICIENT.
AC(20)	0.0	FIXED THRUST STRUCTURE WEIGHT.
AC(21)	0.0	INSULATION WEIGHT COEFFICIENT.
AC(22)	0.0	COVER PANEL WEIGHT CCEFFICIENT.
AC(23)	0.0	LAUNCH GEAR WEIGHT COEFFICIENT.
AC(24)	0.0	FIXED LAUNCH GEAR WEIGHT.
AC(25)	0.31	LANDING GEAR WEIGHT COEFFICIENT.
AC(26)	0.0	LANDING GEAR WEIGHT COEFFICIENT.
AC(27)	0.0	FIXED LANDING GEAR WEIGHT.
AC(28)	0.00766	ROCKET ENGINE WEIGHT COEFFICIENT.
AC(29)	0.00033	ROCKET ENGINE WEIGHT COEFFICIENT.
AC(30)	0.5	ROCKET ENGINE WEIGHT EXPONENT.
AC(31)	130.0	FIXED ROCKET ENGINE WEIGHT.
AC(32)	1782.63	TURBORAMJET ENGINE WEIGHT COEFFICIENT (LOWER DESIGN PCINT).
AC(33)	0.003	TURBORAMJET ENGINE WEIGHT EXPONENT (LOWER DESIGN PCINT).
AC(34)	1594.53	TURBORAMJET ENGINE WEIGHT COEFFICIENT (UPPER DESIGN POINT).
AC(35)	0.0032	TURBORAMJET ENGINE WEIGHT EXPCNENT (UPPER DESIGN POINT).
AC(36)	0.53	FUEL TANK WEIGHT COEFFICIENT.
AC(37)	0.0	FIXED FUEL TANK WEIGHT.
AC(38)	1.25	OXIDIZER TANK WEIGHT COEFFICIENT.
AC(39)	0.0	FIXED OXIDIZER TANK WEIGHT.
AC(40)	0.59	FUEL TANK INSULATION WEIGHT CCEFFICIENT.
AC(41)	0.0	FIXED FUEL TANK INSULATION WEIGHT.
AC(42)	0.23	OXIDIZER TANK INSULATION WEIGHT COEFFICIENT.
AC(43)	0.0	FIXED OXIDIZER TANK INSULATION WEIGHT.
AC(44)	0.0	FUEL SYSTEM WEIGHT CCEFFICIENT.
AC(45)	0.0	FUEL SYSTEM WEIGHT COEFFICIENT.

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# WAATS WEIGHT COEFFICIENTS AND EXPONENTS

COEF.	COMPILED VALUE	DEFINITION
AC(46)	0.0	FIXED FUEL SYSTEM WEIGHT.
AC(47)	0.0	OXIDIZER SYSTEM WEIGHT COEFFICIENT.
AC(48)	0.0	OXIDIZER SYSTEM WEIGHT COEFFICIENT.
AC(49)	0.0	FIXED OXIDIZER SYSTEM WEIGHT.
AC(50)	0.45	FUEL TANK PRESSURE SYSTEM WEIGHT COEFFICIENT.
AC(51)	2.45	OXIDIZER TANK PRESSURE SYSTEM WEIGHT COEFFICIENT.
AC(52)	0.0	FIXED PRESSURE SYSTEM WEIGHT.
AC(53)	4.345	INLET WEIGHT COEFFICIENT.
AC(54)	1.0	INLET WEIGHT EXPONENT.
AC(55)	0.0	GIMBAL SYSTEM WEIGHT COEFFICIENT.
AC(56)	0.0	FIXED GIMBAL SYSTEM WEIGHT.
AC(57)	78.5	ATTITUDE CONTROL SYSTEM SYSTEM WEIGHT COEFFICIENT.
AC(58)	0.079	ATTITUDE CONTROL SYSTEM SYSTEM WEIGHT EXPONENT.
AC(59)	0.0	FIXED ATTITUDE CONTROL SYSTEM SYSTEM WEIGHT.
AC(60)	0.323	AERODYNAMIC CONTROL SYSTEM WEIGHT COEFFICIENT.
AC(61)	0.0	FIXED AERODYNAMIC CONTROL SYSTEM WEIGHT.
AC(62)	0.0	SEPARATION SYSTEM WEIGHT COEFFICIENT.
AC(63)	0.0	FIXED SEPARATION SYSTEM WEIGHT.
AC(64)	0.10	ATTITUDE CONTROL SYSTEM TANK WEIGHT COEFFICIENT.
AC(65)	0.0	FIXED ATTITUDE CONTROL SYSTEM TANK WEIGHT.
AC(66)	1.167	ELECTRICAL SYSTEM WEIGHT COEFFICIENT.
AC(67)	0.0	FIXED ELECTRICAL SYSTEM WEIGHT.
AC(68)	2.64	HYDRAULIC/PNEUMATIC SYSTEM WEIGHT COEFFICIENT.
AC(69)	0.0	FIXED HYDRAULIC/PNEUMATIC SYSTEM WEIGHT.
AC(70)	66.37	AVIONIC SYSTEM WEIGHT COEFFICIENT.
AC(71)	0.0	FIXED AVIONIC SYSTEM WEIGHT.
AC(72)	220.0	CREW WEIGHT COEFFICIENT.
AC(73)	0.0	FIXED CREW WEIGHT.
AC(74)	0.0	CREW PROVISIONS WEIGHT COEFFICIENT.
AC(75)	0.0	FIXED CREW PROVISIONS WEIGHT.
AC(76)	0.0	FIXED INSULATION WEIGHT.
AC(77)	0.0	FIXED COVER PANEL WEIGHT.
AC(78)	0.608	WING WEIGHT EXPONENT.
AC(79)		NOT USED.
AC(80)	0.0	CREW PROVISIONS WEIGHT COEFFICIENT.
AC(81)	1.0	BODY WEIGHT EXPONENT.
AC(82)	0.1	RAMJET ENGINE WEIGHT COEFFICIENT.
AC(83)	0.0	FIXED RAMJET ENGINE WEIGHT.
AC(84)	0.0	RESERVE FUEL WEIGHT COEFFICIENT.
AC(85)	0.0	FIXED RESERVE FUEL WEIGHT.
AC(86)	0.0	RESERVE OXIDIZER WEIGHT COEFFICIENT.
AC(87)	0.0	FIXED RESERVE OXIDIZER WEIGHT.
AC(88)		NOT USED.
AC(89)	1.09	VERTICAL TAIL WEIGHT EXPONENT.
AC(90)	1.0	HORIZONTAL TAIL WEIGHT EXPONENT.
AC(91)	0.0	FIXED TURBOCRAMJET ENGINE WEIGHT.
AC(92)	0.0	RESIDUAL FUEL WEIGHT COEFFICIENT.

# WAATS WEIGHT COEFFICIENTS AND EXPONENTS

COEF.	COMPILED VALUE	DEFINITION
AC(93)	0.0	FIXED RESIDUAL FUEL WEIGHT.
AC(94)	0.0	RESIDUAL OXIDIZER WEIGHT COEFFICIENT.
AC(95)	0.0	FIXED RESIDUAL OXIDIZER WEIGHT.
AC(96)	0.0	ATTITUDE CONTROL SYSTEM PROPELLANT WEIGHT COEFFICIENT.
AC(97)	0.0	FIXED ATTITUDE CONTROL SYSTEM PROPELLANT WEIGHT.
AC(98)	0.0	CONTINGENCY AND GROWTH WEIGHT COEFFICIENT.
AC(99)	0.0	FIXED CONTINGENCY AND GROWTH WEIGHT.
AC(100)		NOT USED.
AC(101)	0.795	LANDING GEAR WEIGHT EXPONENT.
AC(102)	0.0001	ENGINE MOUNT WEIGHT COEFFICIENT.
AC(103)	0.0	FIXED ENGINE MOUNT WEIGHT.
AC(104)	0.316	FUEL DISTRIBUTION SYSTEM WEIGHT COEFFICIENT.
AC(105)	0.0	FIXED INLET WEIGHT.
AC(106)	117.35	RAMP WEIGHT COEFFICIENT.
AC(107)	0.294	RAMP WEIGHT EXPONENT.
AC(108)	0.0	FIXED RAMP WEIGHT.
AC(109)	0.0	SPIKE WEIGHT COEFFICIENT.
AC(110)	1.0E-6	GIMBAL SYSTEM WEIGHT EXPONENT.
AC(111)	0.903	AERODYNAMIC CONTROL SYSTEM WEIGHT EXPONENT.
AC(112)	1.0	ELECTRICAL SYSTEM WEIGHT EXPONENT.
AC(113)	1.0	HYDRAULIC/PNEUMATIC SYSTEM WEIGHT EXPONENT.
AC(114)	0.361	AVIONIC SYSTEM WEIGHT EXPONENT
AC(115)	0.0	RESIDUAL ATTITUDE CONTROL SYSTEM PROPELLANT WEIGHT COEFFICIENT.
AC(116)	0.0	PROPELLANT INFLIGHT LOSS WEIGHT COEFFICIENT.
AC(117)	0.0	WING WEIGHT COEFFICIENT.
AC(118)	1.0E-6	WING WEIGHT EXPONENT.
AC(119)	0.0	HORIZONTAL TAIL WEIGHT COEFFICIENT.
AC(120)	1.0E-6	HORIZONTAL TAIL WEIGHT EXPONENT.
AC(121)	1.0E-6	LANDING GEAR WEIGHT EXPONENT.
AC(122)	0.0	AERODYNAMIC CONTROL SYSTEM WEIGHT COEFFICIENT.
AC(123)	1.0E-6	AERODYNAMIC CONTROL SYSTEM WEIGHT EXPONENT.
AC(124)	0.0	ATTITUDE CONTROL SYSTEM WEIGHT COEFFICIENT.
AC(125)	1.0E-6	ATTITUDE CONTROL SYSTEM WEIGHT EXPONENT.
AC(126)	0.0	ELECTRICAL SYSTEM WEIGHT COEFFICIENT.
AC(127)	1.0E-6	ELECTRICAL SYSTEM WEIGHT EXPONENT.
AC(128)	0.0	HYDRAULIC/PNEUMATIC SYSTEM WEIGHT COEFFICIENT.
AC(129)	0.0	HYDRAULIC/PNEUMATIC SYSTEM WEIGHT COEFFICIENT.
AC(130)	0.0	INTEGRAL FUEL TANK WEIGHT COEFFICIENT.
AC(131)	0.0	FIXED INTEGRAL FUEL TANK WEIGHT.
AC(132)	0.0	INTEGRAL OXIDIZED TANK WEIGHT COEFFICIENT.
AC(133)	0.0	FIXED INTEGRAL OXIDIZER TANK WEIGHT.
AC(134)	0.0	ATTITUDE CONTROL SYSTEM FUEL WEIGHT COEFFICIENT.

### Input Data Forms

Input data forms are shown on the following pages for both the design data and the weight coefficients and exponents. Two types of forms were originally considered. The first type consisted of ten separate forms for the ten possible paths through the program. The other type, which is the one shown, has provisions for all ten paths on a single set of forms. The first column of these forms are the variable names, which can be correlated with the definitions given on the preceding pages, and the second column gives the compiled values of these variables. The remaining ten columns provide blocks for entering the values of the variables. If a block is filled with X's, a value is not required.

[illegible]

## WAATS INPUT DATA - DESIGN DATA

NAVIS INPUT DATA - DESIGN DATA					
TENG	1				3
	1		2		
ICRY	1	2	1	2	2
ISHAPE					
SFUJK	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
SHURZ	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
SJATK	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
SIPS	0.0				
SISPAN	0.0				
SVEIT	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
SWING	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
TANKS	1.0				
THRUST	0.0				
TPDCT	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
TYTAIL	1.25				
VFUJK	0.0				
VIXTK	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
WAREN	0.0				
WEANDI	0.0				
WPAYLO	0.0				
WPMAIN	0.0				
WFOIN	0.0				
XENLCT	1.0				
ATF	4.0				

# NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

VEHICLE DESIGNATION									
1ENG	1				2				3
ICRY	1		2		1		2		2
ISHAPE	1	2	1	2	1	2	1	2	1
1 2905.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
2 0.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
3 0.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
4 5.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
5 0.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
6 0.00035	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
7 0.0	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX
8 0.0									
9 0.0									
14 0.0									
15 0.341									
16 0.0									
17 0.98									
18 0.0									
19 0.0025									
20 0.0									
21 0.0									
22 0.0									
23 0.0									
24 0.0									
25 0.41									
26 0.0									

[illegible]



NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	1										2						3		
	1					2					1			2			2		
	1	2	1	2	1	1	2	1	2	1	1	2	1	2	1	2	1	2	2
ICPY																			
ISHAPE																			
50	0.45	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			
51	2.45	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			
52	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			
53	4.345																		
54	1.0																		
55	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			
56	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			
57	78.5																		
58	0.079																		
59	0.0																		
60	0.323																		
61	0.0																		
62	0.0																		
63	0.0																		
64	0.10																		
65	0.0																		
66	1.167																		
67	0.0																		
68	2.64																		
69	0.0																		
70	66.37																		
71	0.0																		
72	220.0																		



HAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	1						2						3					
	1			2			1			2			2			1		
	1	2		1	2		1	2		1	2		1	2		1	2	
100																		
101																		
102																		
103																		
104																		
105																		
106																		
107																		
108																		
109																		
110																		
111																		
112																		
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114																		
115																		
116																		
117																		
118																		
119																		
120																		
121																		



### Example Problem

The hypersonic cruise transport (HST) studied in ref. 8 was chosen to demonstrate the use of WAATS. The basic configuration (Fig. 1) is a blended wing-body with a single vertical tail. The fuselage and wing are actively-cooled aluminum alloy, while the vertical tail is uncooled Inconel 718 (Table I). A water-glycol coolant is circulated through passages in the wing and fuselage skins. Heat shields are also used on the lower surface of the wing aft of the leading edge and on the portions of the fuselage with the highest heat loads.

The propulsion system consists of four turbofan ramjet engines and nine variable-geometry scramjets. The turbojet engines are used from takeoff to Mach 3, at which point the adjustable inlet door (Fig. 1) closes off the turbojet ducting. The ramjet engines operate from low transonic Mach numbers to the Mach 6 cruise condition, with subsonic combustion at the lower Mach numbers and supersonic combustion at cruise.

The fuel for both propulsion systems is liquid hydrogen carried in two tanks, one forward and one aft of the passenger/cargo compartment. The non-integral tanks are of multicell or "pillow" construction (Fig. 1). The material is Inconel 718. Polyurethane foam insulation is used for thermal insulation of the tanks. The fuel is also used as a heat sink for the fuselage, wing and scramjet cooling systems.

Tables I and II (reproduced from ref. 8) give the majority of the data required for the analysis. Additional data will be presented as it is used.

The preparation of the input data forms will be discussed first. This will be followed by the input and output listings and a comparison of the WAATS Weight Statement with the HST Weight Summary given in ref. 8.

Design Data. -- The input data forms are shown on pages 52 - 59. Since the HST has two types of engines and WAATS allows the specification of only one type of engine, a choice had to be made as to the basic engines for the analysis. The turbojet engines (ICRY = 1) were selected because the weight calculations for these engines are complex, while the ramjet engine weight can be easily calculated and input as a fixed weight. The fuel being liquid hydrogen gives ICRY = 2. The vehicle shape (Fig. 1) is that of an aircraft, so ISHAPE = 2. These three parameters define the applicable column in the input data forms. The entries in the forms consist of asterisks, if the compiled value is used, and the values to be used, when the compiled values are not to be used.

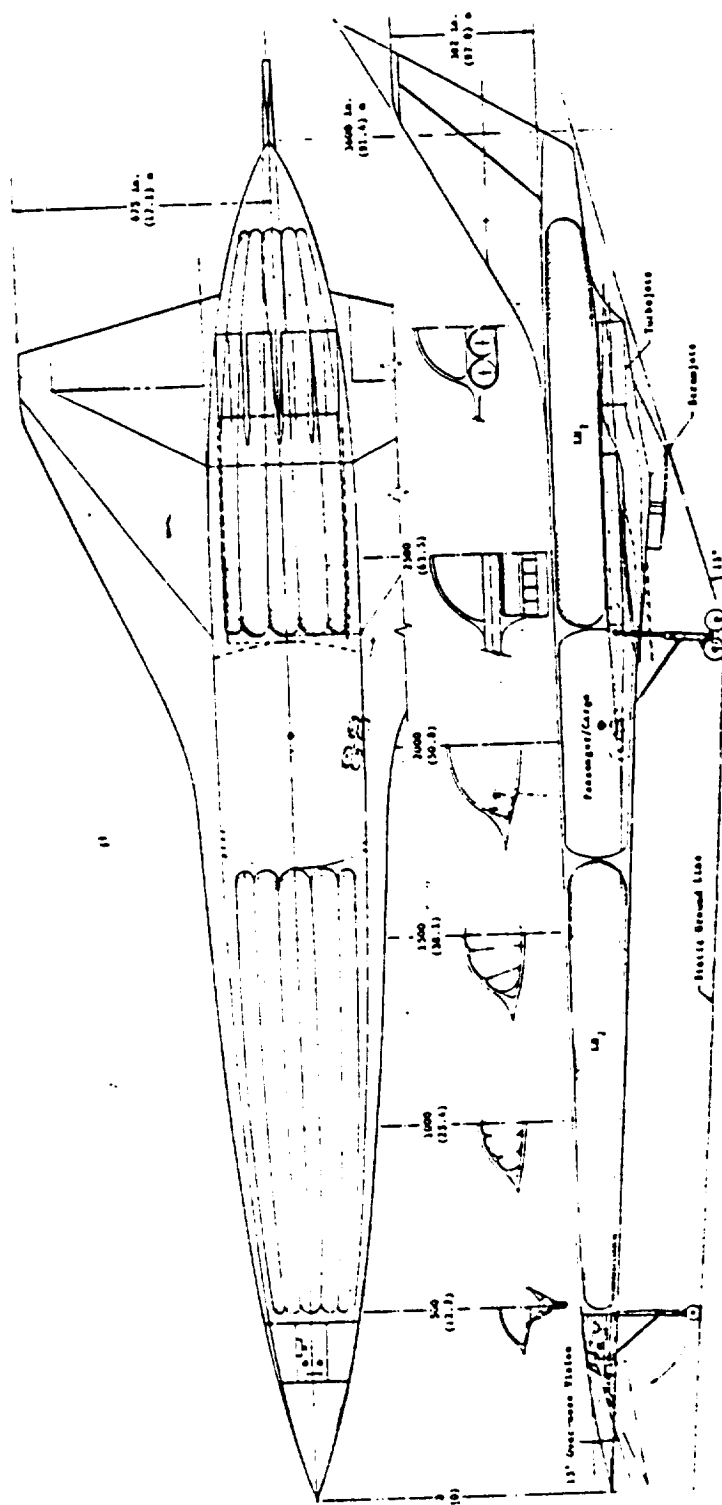


Figure 1. - Baseline Hypersonic Transport

TABLE I  
BASELINE HST SUMMARY CHARACTERISTICS

Mission

Cruise Mach number . . . . .	6.0
Payload weight . . . . .	22 700 kg (50 000 lb)
Payload volume . . . . .	453 m <sup>3</sup> (16 000 ft <sup>3</sup> )

Performance

Fuel . . . . . liquid hydrogen

Operations

Flight cycles for structural design . . . . . 20 000

Vehicle

Aero configuration: blended wing-body with single vertical tail per reference 2, modified to enhance precompression and accommodate propulsion system installation.

General arrangement: non-integral fuel tanks fore and aft; centrally located payload compartment.

Accelerator/loiter engines: four P6W STF-230A-type  
Cruise/accelerator engines: horizontal array of dual-combustion-mode, variable-geometry scramjets

Design and structures

Wing: actively-cooled aluminum alloy per reference 4  
Vertical tail: uncooled Inconel 718 per reference 4  
Fuselage: actively-cooled aluminum alloy per reference 3  
Scramjets: actively-cooled, two-dimensional modules  
Propulsion installation: per reference 6  
Fuel tanks: multicell Inconel 718 per reference 3  
Thermal management: airframe cooling system and operating temperatures per reference 4, 5 and 6; external heat shields on portions of wing and fuselage to reduce cooling load per references 3, 4 and 5; hermetically sealed polyurethane foam insulation system for fuel tanks.

Weight

Gross take-off weight of 218 400 kg (481 400 lb)

Technology level

Presently postulated or immediately foreseeable

TABLE II  
AIRPLANE CONFIGURATION AND WEIGHT SUMMARY DATA

Fuselage length, $l_F$ . . . . .	91.4 m (300 ft)
Reference area (projected wing), $S$ . . . . .	$866 \text{ m}^2$ ( $9323 \text{ ft}^2$ )
Wing loading at take-off, $(W/S)_{GTO}$ . . . . .	$252 \text{ kg/m}^2$ ( $51.6 \text{ lb/ft}^2$ )
Wing thickness ratio, $t/c$ . . . . .	0.03
Vertical tail area, $S_V$ . . . . .	$94.8 \text{ m}^2$ ( $1020 \text{ ft}^2$ )
Payload compartment volume . . . . .	$453 \text{ m}^3$ ( $16\ 000 \text{ ft}^3$ )
Total fuel tank volume . . . . .	$1020 \text{ m}^3$ ( $36\ 000 \text{ ft}^3$ )
Total turbojet thrust (S.L. static), $T_{TJ} \ N_{TJ}$ . . . . .	1 032 000 N (232 000 lb)
Maximum thrust-weight ratio at take-off, $(T/W)_{GTO}$ . . . . .	0.482
Scramjet module size: 0.927 m x 0.927 m (3.04 ft x 3.04 ft) inlets 6.4 m (21 ft) length	
Dry airplane weight, $W_e$ . . . . .	123 200 kg (271 600 lb)
Fuel weight, $W_{f_T}$ . . . . .	69 400 kg (153 000 lb)
Gross take-off weight, $W_{GTO}$ . . . . .	218 400 kg (481 400 lb)
Dry airframe/gross take-off weight, $W_e/W_{GTO}$ . . . . .	0.5641
Payload/gross take-off weight, $W_{PL}/W_{GTO}$ . . . . .	0.1038
Main fuel/gross take-off weight, $W_{f_T}/W_{GTO}$ . . . . .	0.3173



The inlet capture area (AICAPT) is not specified in ref. 8 for the turbojet engines. From Fig. 1, however, it appears to be approximately equal to capture area of the ramjets, which is 83.2 ft<sup>2</sup> (Table II), so this value will be used. Also from Fig. 1, it appears from the flight deck layout that there are provisions for three crew members (CREW = 3.). The altitudes at the beginning and end of cruise are given on page 2-31 of ref. 8; the latter (DH = 94 600 ft) was chosen as the design altitude. The design Mach number (DM = 6.) is given in Table I, while the fuselage length (ELBODY = 300. ft) is given in Table II. The inlet and ramp lengths (ELNLET = 53. ft and ELRAMP = 20. ft) were scaled from Fig. 1. The Mach number factor (FCTMOK = 1.5) and the geometrical out of round factor (GEOFCT = 1.33) used in calculating the duct weight are defined in ref. 5, page 57.

The geometric span (GSPAN = 112.5 ft) is shown in Fig. 1, and the maximum body height (HBODY = 16. ft) was scaled from the same figure. Since the fuel is liquid hydrogen, with no oxidizer, the oxidizer to fuel mixture ratio (OF) must be set to zero. The maximum dynamic pressure (QMAX = 948. lb/ft<sup>2</sup>) was taken from ref. 8, page 2-34. The surface area of the body (SBODY = 19 000. ft<sup>2</sup>) was approximated by scaling Fig. 1, as was the surface area of the fuel tank (SFUTK = 4500. ft<sup>2</sup>). The vertical tail area (SVERT = 1020. ft<sup>2</sup>) and the wing area (SWING = 9323. ft<sup>2</sup>) are given in Table II.

Ref. 8, page 2-33, states that heat shields are used on the lower surface of the wing and fuselage, but does not give the total area. However, it does specify the unit weight as 0.9 lb/ft<sup>2</sup> and the total weight is given in Table III as 10 200 lb; therefore;

$$\text{STPS} = 10\,200. / 0.9 = 11\,333. \text{ ft}^2$$

The structural span (STSPAN = 109.5 ft) and the wing thickness at the root (TROOT = 3.3 ft) were scaled from Fig. 1. The tail type coefficient's (TYTAIL = 1.) was assumed to be that for a conventional tail (ref. 5, page 71). The fuel tank volume (VFUTK = 36 000. ft<sup>3</sup>) is given in Table II. The reference engine airflow (WAREF = 400. lb/sec) was chosen arbitrarily and is discussed in a later section. The estimated landing weight (WLANDI = 400 000. lb) and the estimated takeoff weight (WTOIN = 500 000. lb) were also chosen arbitrarily. The payload weight (WPAYLD = 50 000. lb) is given in Table I.

The main propellant weight is given in Table II as 153 000. lb. This includes a climb fuel fraction (K<sub>CL</sub> = 0.40), a descent fuel fraction (K<sub>D</sub> = 0.02) and a reserve fuel fraction (K<sub>R</sub> = 0.10); which leaves 48 percent of the total fuel for cruise (ref. 8, pages 2-22 and 2-27). WAATS has provisions for a main impulse propellant weight and a reserve fuel weight coefficient. For

this example these are taken as  $WPMAIN = 136\ 000\text{ lb}$  and  $AC(84) = 0.125$ , to give the correct total propellant weight.

Ref. 8 does not specify the load factors. However, much of the data used in this reference is derived from refs. 22 - 24. In ref. 22, page 159; a vertical load factor of +2.0 g with an ultimate factor of safety of 1.5 is specified. These values will be used to give  $XLF = 3$ .

Weight Coefficients and Exponents. -- As can be seen from the input data forms, the compiled values are used for the majority of the weight coefficients and exponents. Therefore, only the equations for which the compiled values are superseded will be discussed. The equations will be considered in the order in which they appear in ref. 5.

Wing and Body Structure: The compiled values are those for high speed aircraft with high temperature construction. Provisions are not made for the actively-cooled aluminum structure of the HST; therefore, the compiled values will be used.

Thrust Structure: The equation for the thrust structure for airbreathing engines is given in Fig. 3.2-3 of ref. 5 as

$$WT = 0.00625(TTOT) + 69$$

Thus  $AC(19) = 0.00625$  and  $AC(20) = 69$ .

Thermal Protection System Cover Panels: The unit weight of the heat shields was specified in the preceding section, i.e.,  $AC(22) = 0.9$ .

Landing Gear: The landing gear weight is assumed to be a function of the landing weight, not the takeoff weight; therefore, from ref. 5, Fig. 3.4-2,  $AC(26) = 0.00916$  and  $AC(121) = 1.124$ . Note that  $AC(25)$  and  $AC(101)$  must be set to zero.

Engines: The compiled values of the coefficients and exponents were used to calculate the weight of the turbojet engines. The airflow through the engines ( $WA = WAREF * ACTR$ ) could not be calculated from the available data, so they were assumed ( $WAREF = 400\text{ lb/sec}$  and  $ACTR = 1$ .) to make the engine weight approximately equal to that given in ref. 8. The weight of the ramjet engines is included as a fixed engine weight by using  $AC(82) = 0.1$  and dividing the result by four to get an equivalent fixed weight per turbojet engine, i.e.,

$$AC(91) = 0.1 \times 157\ 000. / 4. = 3925\text{ lb/engine}$$

Engine Mounts: The engine mount weight coefficient (AC(102) = 0.004) suggested in ref. 5, page 41, was used.

Fuel Tank Insulation: The basic fuel tank insulation weight coefficient was calculated using the equation in Fig. 3.5-6 in ref. 5 and the suggested radiating temperature of 500°F, giving

$$AC(40) = 0.0007(500.) + 0.24 = 0.59$$

This was then corrected for flight duration using Fig. 3.5-7. Note that the maximum time on this curve is 7000. sec, while the flight time specified for the HST is 7200. sec. Therefore, the maximum value on the curve was used, giving

$$AC(40) = 0.59 \times 1.04 = 0.61$$

Fuel System: The equation for the fuel system weight given in ref. 5, page 52, is

$$WFUSYS = AC(44) * TTOT + AC(45) * ELBODY + AC(46)$$

The weight coefficients AC(44) and AC(45) are given in Fig. 3.5-9, where the maximum thrust is only 100 000. lb. Equations were written for these curves, but the values calculated for a thrust of 232 000. lb were not realistic, so ref. 11 was consulted. This reference (pages 55 - 56) recommends values of AC(44) = 0.0015 to 0.003 for liquid hydrogen and AC(45) = 0. The largest recommended value (AC(44) = 0.003) is used.

Pressurization Systems: The weight of the fuel pressurization system is given in Fig. 3.5-11 of ref. 5 as

$$WT = 0.45 * VFUTK$$

This equation gives a very high weight for the system. Ref. 11, Fig. 5.1-7, page 60, shows a carpet plot of the equivalent weight coefficient. At liquid hydrogen storage temperature and a pressure of 25 psi (ref. 2, page 2-37), the coefficient is approximately one-tenth of the coefficient in the equation above. This value (AC(50) = 0.045) is used.

Attitude Control System: Ref. 8 does not mention an attitude control system for the HST, so AC(57) and AC(58) were set to zero.

Crew Provisions: Table 3.9-1 of ref. 5 was used to select these coefficients. The equipment environmental control weight coefficient (AC(74) = 0.0005) was taken directly from the table.

The fixed crew provisions weight ( $AC(75) = 400.$ ) was taken as the sum of the items in the third column of the table. The crew provisions weight coefficient ( $AC(80) = 260.$ ) was taken as the sum of a 100-lb seat and the remaining items in column 2 of the table.

Trapped Fuel: Ref. 5, page 80, gives a range of  $AC(92) = 0.005$  to  $0.03$ . The average value ( $AC(92) = 0.018$ ) was used.

Reserve Fuel: See the discussion on the main propellant weight in the previous section.

Inflight Losses: The inflight loss fraction is assumed to be  $AC(116) = 0.028$  to give the same losses as predicted in ref. 8.

# NAATS INPUT DATA - DESIGN DATA

## VEHICLE DESIGNATION: HYPERSONIC CRUISE TRANSPORT

ITEM	1			2			3		
	1		2	1		2	1		2
	1	2		1	2		1	2	
ICRY	2								
ISHAPE	2								
ACTH	1.0		*						
AICAPT	0.0		83.2						
ARATIO	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
CREW	2.0		3.						
DH	0.0		94600.						
DN	1.0		6.						
LLRCOV	0.0		300.						
ELNLET	0.0		58.						
CLRAMP	6.0		20.						
ENGIN5	2.0		4.						
FCTMLK	1.0		1.5						
GEFECT	1.0		1.33						
GSPAN	0.0		112.5						
HHDDY	1.0		16.0						
UF	6.0	XXXXXXXXXX	0.			XXXXXXXXXX			
UFACS	0.0		*						
PCNAM	1000.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX
PHIGHT	176.0		*						
PLNM	46.0		*						
QYAX	0.0		948.						
SDDY	0.0		19000.						
SFAIR	0.0		*						

### HAATS INPUT DATA - DESIGN DATA

*[The page contains extremely faint, illegible markings and noise.]*

# NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

## HYPERSONIC CRUISE TRANSPORT

VEHICLE DESIGNATION		1				2				3			
ICPY	ICPY	1		2		1		2		1		2	
		1	2	1	2	1	2	1	2	1	2	1	2
1	2905.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
2	0.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
3	0.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
4	5.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
5	0.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
6	0.00035	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
7	0.0	XXXXXXXXXX		XXXXXXXXXX	*	XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	
8	0.0				*								
9	0.0				*								
14	0.0				*								
15	0.341				*								
16	0.0				*								
17	0.98				*								
18	0.0				*								
19	0.0025				0.00625								
20	0.0				69:								
21	0.0				*								
22	0.0				0.9								
23	0.0				*								
24	0.0				*								
25	0.31				0.								
26	0.0				0.00916								

HAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	ICPV	ISHAPE	1						2						3					
			1			2			1			2			1			2		
			1	2		1	2	*	1	2		1	2		1	2		1	2	
27	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
28	0.00766		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
29	0.00033		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
30	0.5		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
31	130.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
32	1782.63							*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	
33	0.003							*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	
34	1994.53							*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	
35	0.0032							*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	
36	0.53							*												
37	0.0							*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
38	1.25		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
39	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
40	0.59		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	0.61	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
41	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
42	0.23		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
43	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
44	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	0.003	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
45	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
46	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
47	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
48	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				
49	0.0		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX				



NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	ICPV	ISHAPE	1				2				3			
			1		2		1	2	1		2		1	2
			1	2	1	2			1	2	1	2		
50		0.45	XXXXXXXXXX	XXXXXXXXXX		0.045	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				
51		2.45	XXXXXXXXXX	XXXXXXXXXX		*	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				
52		0.0	XXXXXXXXXX	XXXXXXXXXX		*	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				
53		4.345				*								
54		1.0				*								
55		0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX		
56		0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX		
57		78.5				0.								
58		0.074				0.								
59		0.0				*								
60		0.323				*								
61		0.0				*								
62		0.0				*								
63		0.0				*								
64		0.10				*								
65		0.0				*								
66		1.167				*								
67		0.0				*								
68		2.64				*								
69		0.0				*								
70		66.37				*								
71		0.0				*								
72		220.0				*								

NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	1				2				3	
	1		2		1		2		2	
	1	2	1	2	1	2	1	2	1	2
73	0.0					*				
74	0.0					0.0005				
75	0.0					400.				
76	0.0					*				
77	0.0					*				
78	0.608					*			XXXXXXXXXX	
80	0.0					260.				
81	1.0					*				
82	0.1					XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX
83	0.0					XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX
84	0.0					XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX
85	0.0					0.125				
86	0.0					*			XXXXXXXXXX	
87	0.0					*			XXXXXXXXXX	
88	1.09					*			XXXXXXXXXX	XXXXXXXXXX
89	1.0					*			XXXXXXXXXX	XXXXXXXXXX
90	0.0					3925.			XXXXXXXXXX	XXXXXXXXXX
91	0.0					0.018			XXXXXXXXXX	XXXXXXXXXX
92	0.0					*				
93	0.0					*			XXXXXXXXXX	
94	0.0					*			XXXXXXXXXX	
95	0.0					*			XXXXXXXXXX	
96	0.0					*				
97	0.0					*				

WAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	1				2				3			
	1		2		1		2		1		2	
	1	2	1	2	1	2	1	2	1	2	1	2
ICRY												
ISHAPE												
98		0.0				*						
99		0.0				*						
101		0.795				0.						
102		0.0001				0.004						
103		0.0				*						
104		0.316				XXXXXXXXXX						
105		0.0				*						
106		117.35				*						
107		0.294				*						
108		0.0				*						
109		0.0				*						
110		1.0E-6				XXXXXXXXXX						
111		0.903				*						
112		1.0				*						
113		1.0				*						
114		0.361				*						
115		0.0				*						
116		0.0				0.0316						
117		0.0				XXXXXXXXXX						
118		1.0E-6				XXXXXXXXXX						
119		0.0				XXXXXXXXXX						
120		1.0E-6				XXXXXXXXXX						
121		1.0E-6				1.124						

MAAT3 INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS												
ITEM		1				2				3		
		1		2		1		2		1		2
ICRY												
ISHAPE		1	2	1	2	1	2	1	2	1	2	
122	0.0				*							
123	1.0E-6				*							
124	0.0				*							
125	1.0E-6				*							
126	0.0				*							
127	1.0E-6				*							
128	0.0				*							
129	0.0				*							
130	0.0				*							
131	0.0				*							
132	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
133	0.0	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	*	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
134	0.0				*							

Input and Output Listings. -- The input data listing is shown on the next page, followed by the output listing. The input data was taken directly from the input data forms, except that the number of fuel tanks (TANKS = 2.0) is specified. This number is not used; but since there are two tanks (Fig. 1) and the number is printed in the output, it was included.

The output consists of the NAMELIST listing, a list of the non-zero weight coefficients, two tables of the design data, a mass iteration table and the Weight Statement. The NAMELIST listing is superfluous, since all of the input data is also printed in the list of non-zero weight coefficients or the tables of design data. The mass iteration table shows the principal weights at the end of each iteration loop. If reasonable values are used for the estimated takeoff and landing weights, the convergence is very rapid.

# INPUT DATA - HST EXAMPLE

```

&INWAP IENG=1,
AICAPT=83.2,
CREW=3.0,
DH=94600.0,
DM=6.0,
ELBODY=300.0,
ELALET=58.0,
ELRAMP=20.0,
ENGINS=4.0,
FCTMOK=1.5,
GEOFCT=1.33,
GSPAN=112.5,
HBODY=16.0,
CF=0.0,
QMAX=948.0,
SBCDY=19000.0,
SFUTK=4500.0,
STPS=11333.0,
STSPAN=109.5,
SVERT=1020.0,
SWING=9323.0,
TANKS=2.0,
THRUST=58000.0,
TRCOT=3.3,
TYTAIL=1.0,
VFUTK=36000.0,
WAREF=400.0,
WLANDI=40000.0,
WPAYLD=50000.0,
WPMIN=136000.0,
WTCIN=500000.0,
XLF=3.0,
AC(19)=0.00625,
AC(20)=69.0,
AC(22)=0.9,
AC(25)=0.0,
AC(26)=0.00916,
AC(40)=0.61,
AC(44)=0.003,
AC(50)=0.045,
AC(57)=0.0,
AC(58)=0.0,
AC(74)=0.0005,
AC(75)=400.0,
AC(80)=260.0,
AC(84)=0.125,
AC(91)=3925.0,
AC(92)=0.018,
AC(101)=0.0,
AC(102)=0.004,
AC(116)=0.0316,
AC(121)=1.124,&END

```



# NCN-ZERO WEIGHT CCEFFICIENTS

AC( 1) = 2905.00  
 AC( 4) = 5.00000  
 AC( 6) = .350000E-03  
 AC( 15) = .341000  
 AC( 17) = .980000  
 AC( 19) = .625000E-02  
 AC( 20) = 69.0000  
 AC( 22) = .900000  
 AC( 26) = .916000E-02  
 AC( 28) = .766000E-02  
 AC( 29) = .330000E-03  
 AC( 30) = .500000  
 AC( 31) = 130.000  
 AC( 32) = 1782.63  
 AC( 33) = .300000E-02  
 AC( 34) = 1994.53  
 AC( 35) = .320000E-02  
 AC( 36) = .530000  
 AC( 38) = 1.25000  
 AC( 40) = .610000  
 AC( 42) = .230000  
 AC( 44) = .300000E-02  
 AC( 50) = .450000E-01  
 AC( 51) = 2.45000  
 AC( 53) = 4.34500  
 AC( 54) = 1.00000  
 AC( 60) = .323000  
 AC( 64) = .100000  
 AC( 66) = 1.16700  
 AC( 68) = 2.64000  
 AC( 70) = 66.3700  
 AC( 72) = 220.000  
 AC( 74) = .500000E-03  
 AC( 75) = 400.000  
 AC( 78) = .608000  
 AC( 80) = 260.000  
 AC( 81) = 1.00000  
 AC( 82) = .100000  
 AC( 84) = .125000  
 AC( 89) = 1.09000  
 AC( 90) = 1.00000  
 AC( 91) = 3925.00  
 AC( 92) = .180000E-01  
 AC(102) = .400000E-02  
 AC(104) = .316000  
 AC(106) = 117.350  
 AC(107) = .294000  
 AC(110) = .100000E-05  
 AC(111) = .903000  
 AC(112) = 1.00000  
 AC(113) = 1.00000  
 AC(114) = .361000



NCN-ZERO WEIGHT COEFFICIENTS

AC(116) = .316000E-01  
AC(118) = .100000E-05  
AC(120) = .100000E-05  
AC(121) = 1.12400  
AC(123) = .100000E-05  
AC(125) = .100000E-05  
AC(127) = .100000E-05

# DESIGN DATA

## WETTED AREAS

GROSS BODY	19000.00
FUEL TANKS	4500.00
OXIDIZER TANKS	0.0

## PLAN AREAS

WING	9323.00
VERTICAL SURFACES	1020.00
HORIZONTAL SURFACES	0.0
FAIRINGS	0.0
THERMAL PROTECTION SYSTEM	11333.00

## DIMENSIONAL DATA

WING GEOMETRIC SPAN	112.50
WING STRUCTURAL SPAN	109.50
WING THICKNESS AT THEORETICAL ROOT	3.30
TOTAL INLET CAPTURE AREA	83.20
ROCKET ENGINE AREA RATIO	0.0
TOTAL INLET LENGTH	58.00
TOTAL RAMP LENGTH	20.00
BODY LENGTH	300.00
BODY HEIGHT	16.00
FUEL TANK VOLUME	36000.00
OXIDIZER TANK VOLUME	0.0

## ENGINE DATA

ENGINE TYPE	TURBORAMJET
NUMBER OF ENGINES	4.00
THRUST OF ONE ENGINE	58000.00
THRUST SCALING FACTOR	1.00
NUMBER OF INLETS	1.00
REFERENCE ENGINE AIRFLOW	400.00
ROCKET ENGINE CHAMBER PRESSURE	1000.00
TURBORAMJET INLET PRESSURE (UPPER)	175.00
TURBORAMJET INLET PRESSURE (LOWER)	46.00

## WEIGHTS

PAYLOAD	50000.00
MAIN IMPULSE PROPELLANT	136000.00
ESTIMATED TAKEOFF WEIGHT	500000.00
ESTIMATED LANDING WEIGHT	400000.00

# DESIGN DATA

## OTHER DESIGN DATA

NUMBER OF CREW	3.00
DESIGN ALTITUDE	94600.00
DESIGN MACH NUMBER	6.00
MACH NUMBER FACTOR	1.50
GEOMETRICAL OUT OF ROUND FACTOR	1.33
OXIDIZER TO FUEL MIXTURE RATIO	0.0
ACS OXIDIZER TO FUEL MIXTURE RATIO	0.0
MAXIMUM DYNAMIC PRESSURE	948.00
NUMBER OF FUSELAGE FUEL TANKS	2.00
TAIL TYPE COEFFICIENT	1.00
ULTIMATE LOAD FACTOR	3.00
PROPELLANT TYPE	CRYOGENIC
SHAPE	AIRCRAFT

MASS ITERATION					
NO	DRY WEIGHT	EMPTY WEIGHT	LANDING WEIGHT	ENTRY WEIGHT	TAKEOFF WEIGHT
1	243798.	243798.	297212.	297212.	454509.
2	235992.	235992.	289406.	289406.	446703.
3	235142.	235142.	288556.	288556.	445853.
4	235049.	235049.	288463.	288463.	445761.

# W E I G H T   S T A T E M E N T

AERODYNAMIC SURFACES		43098.
WING	33584.	
VERTICAL SURFACES	9514.	
HORIZONTAL SURFACES	0.	
FAIRINGS	0.	
BODY STRUCTURE	58110.	78249.
BASIC STRUCTURE	18620.	
SECONDARY STRUCTURE	1519.	
THRUST STRUCTURE	0.	
INTEGRAL FUEL TANKS	0.	
INTEGRAL OXIDIZER TANKS		
ENVIRONMENTAL PROTECTION SYSTEM		10200.
INSULATION	0.	
COVER PANELS	10200.	
LAUNCH AND RECOVERY SYSTEMS		12566.
LAUNCH SYSTEM	0.	
LANDING GEAR	12566.	
MAIN PROPULSION SYSTEM		74708.
ENGINES	42118.	
ENGINE MOUNTS	928.	
FUEL TANKS	19080.	
OXIDIZER TANKS	0.	
FUEL TANK INSULATION	2745.	
OXIDIZER TANK INSULATION	0.	
FUEL SYSTEM	696.	
OXIDIZER SYSTEM	0.	
PROPELLANT PRESSURIZATION SYST	1620.	
INLET SYSTEM	7521.	
ORIENTATION AND SEPARATION SYSTEMS		3166.
GIMBAL SYSTEM	0.	
ATTITUDE CONTROL SYSTEM	0.	
ATTITUDE CONTROL SYSTEM TANKAGE	0.	
AERODYNAMIC CONTROL SYSTEM	3166.	
SEPARATION SYSTEM	0.	
POWER SUPPLY		4393.
ELECTRICAL SYSTEM	3243.	
HYDRAULIC/PNEUMATIC SYSTEM	1150.	
AVIONICS SYSTEM		7267.
CREW SYSTEMS		1403.
DRY WEIGHT		235049.

# W E I G H T   S T A T E M E N T

CRY WEIGHT		235049.
DESIGN RESERVE	0.	
EMPTY WEIGHT		235049.
PAYLOAD	50000.	
CREW	660.	
RESIDUAL PROPELLANTS		2754.
TRAPPED FUEL	2754.	
TRAPPED OXIDIZER	0.	
LANDING WEIGHT		288463.
ATTITUDE CONTROL SYSTEM PROPELLANTS		0.
FUEL	0.	
OXIDIZER	0.	
ENTRY WEIGHT		298463.
MAIN PROPELLANTS		136000.
FUEL	136000.	
OXIDIZER	0.	
RESERVE PROPELLANTS		17000.
FUEL	17000.	
OXIDIZER	0.	
INFLIGHT LOSSES		4298.
TAKEOFF WEIGHT		445761.

Comparison of Results. -- The Weight Summary for the HST is shown in Table III (adapted from ref. 8, page 2-42). Since there is not a one-to-one correspondence between the weight items in the WAATS Weight Statement and the HST Weight Summary, the weight breakdown shown in Table IV will be used for the comparison. Each weight item in the table will be explained and discussed. The Empty Weight, Landing Weight and Takeoff Weight will then be discussed.

**Aerodynamic Surfaces, Controls and Cooling System:** The HST "Aero Structure" weights include the control system, while this is a separate item in the WAATS Weight Statement. Conversely, the cooling system for the wing and fuselage is a separate item in the HST Weight Summary. Thus, the Wing, Vertical Tail and Aerodynamic Control System weights are summed to obtain the total WAATS weight item. The HST Weight item consists of the Wing, Vertical Tail and one-half of the Cooling System weight. The cooling system weight is equally divided between the wing and fuselage, since their wetted areas are almost equal. The resulting weights differ by only two percent.

**Body Structure and Cooling System:** The WAATS Body Structure weight is taken directly from the Weight Statement. The HST weight item includes the Body Structure (Covers, Frames and Compartments), Compartment Insulation and one-half of the Cooling System weight. The WAATS weight is eleven percent larger than the HST weight.

**Environmental Protection System:** This item is identified as Cover Panels in the WAATS Weight Statement and External Shields in the HST Weight Summary. The unit weight and the areas of the cover panels were selected to make these weights equal.

**Launch and Recovery Systems:** The HST landing gear is forty-four percent heavier than the WAATS weight estimate. The correlation curve (Fig. 3.4-2, ref. 5) for landing designed gears shows very good correlation, so the WAATS result is assumed to be a good approximation.

**Engines and Mounts:** The WAATS weight item includes the Engine and Engine Mount Weights, while the HST Weight item consists of the Turbojet and Scramjet weights. The reference engine airflow ( $W_{AREF} = 400$  lb/sec) was arbitrarily selected to give approximately the same weight as the HST estimate. The resulting total weights are within four percent of each other.

**Inlet System:** These items are identified as the Inlet System in the WAATS Weight Statement and as the Turbojet Air Induction in the HST Weight Summary. The HST estimate is almost sixty percent larger than the WAATS estimate. The correlation curves in ref. 5 (Fig. 3.5-12 for the inlet and Fig. 3.5-13 for the ramp)

TABLE III  
WEIGHT SUMMARY - BASELINE HST AIRCRAFT

Group	Item	Weight	
		kg	lb
Aero Structure, $W_W$	Wing	14 800	32 600
	Vertical Tail	3 100	6 900
Body Structure, $W_E$	Covers	15 300	33 600
	Frames	4 700	10 400
Propellant Systems, $W_P$	Compartments	7 900	17 410
	Tanks	15 000	32 900
Thermal Protection, $W_{TP}$	Fuel/Pres/Lub Systems	2 400	5 200
	External Shields	4 600	10 200
Turbojet Propulsion, $W_{TJ}$	Cooling System	6 900	15 300
	Compartment Insulation	500	1 200
Scramjets, $W_{RJ}$	Tank Insulation	3 400	7 590
	Turbojet Engines	11 400	25 000
Avionics, $W_{AV}$	Turbojet Air Induction	5 500	12 000
		7 400	16 200
Equipment, $W_{Equip}$	Launch and Recovery	1 450	3 200
	Prime Power & Distribution	8 200	18 100
	Payload Provisions	3 500	7 800
		7 270	16 000
Dry Airplane, $W_e$		123 000	271 600
Personnel, Residuals and Prime Power Reserve		1 140	2 500
Payload, $W_{PL}$		22 700	50 000
Wet Airplane & Payload		147 000	324 100
In-Flight Losses		2 000	4 300
Main Fuel, $W_{fT}$		69 400	153 000
Gross Take-Off Weight, $W_{GTO}$		218 400	481 400



TABLE IV  
COMPARISON OF WAATS AND HST WEIGHTS

	WAATS	HST
AERODYNAMIC SURFACES, CONTROLS AND COOLING SYSTEM	46 264	47 150
BODY STRUCTURE AND COOLING SYSTEM	78 249	70 260
ENVIRONMENTAL PROTECTION SYSTEM	10 200	10 200
LAUNCH AND RECOVERY SYSTEMS	12 568	18 100
ENGINES AND MOUNTS	43 646	41 200
INLET SYSTEM	7 521	12 000
FUEL TANKS	19 080	32 900
FUEL TANK INSULATION	2 745	7 590
FUEL, PRESSURIZATION AND LUBRICATION SYSTEMS	2 316	5 200
POWER SUPPLY	4 393	7 800
AVIONICS	7 267	3 200
CREW SYSTEMS AND PAYLOAD PROVISIONS	1 403	16 000
EMPTY WEIGHT	<u>235 049</u>	<u>271 600</u>
PAYLOAD	50 000	50 000
CREW AND RESIDUALS	3 414	2 500
LANDING WEIGHT	<u>288 463</u>	<u>324 100</u>
PROPELLANTS	153 000	153 000
INFLIGHT LOSSES	4 298	4 300
TAKEOFF WEIGHT	<u>445 761</u>	<u>481 400</u>

show good correlation. However, the data is for military jets with inlet systems different than that used on the HST. Therefore, the HST estimate is probably the most accurate.

**Fuel Tanks:** The estimated weight of the HST fuel tanks is seventy-two percent larger than the value calculated by WAATS. The only data available in ref. 5 (Fig. 3.5-5) is for an integral fuel tank based on the X-15 concept, while the HST tanks are non-integral. Therefore, the WAATS estimate is open to question.

**Fuel Tank Insulation:** The HST fuel tank insulation weight is almost three times that calculated in WAATS. There is no correlation curve in either of ref. 5 or 11, so the source of the WAATS weight coefficient is not known. The HST weight item includes a helium purge system and hydrogen boil-off during a 30-minute ground hold (ref. 8, page 2-37), but this probably does not entirely account for the large difference.

**Fuel, Pressurization and Lubrication Systems:** The WAATS weight item is obtained by summing the Fuel System and Propellant Pressurization System Weights. The lubrication system is not a separate item in the WAATS Weight Summary, so it is assumed to be included in the engine weight. The HST weight item is taken directly from the Weight Summary. The WAATS weight estimate is again very low, approximately one-half of the HST value. As indicated in the Weight Coefficients and Exponents section, there were questions about the coefficients for both the fuel and pressurization systems; therefore, further study of these coefficients is recommended.

**Power Supply:** In the WAATS Weight Statement, the Power Supply consists of the Electrical System and the Hydraulic/Pneumatic System. In the HST the Prime Power and Distribution consists of (ref. 8, page 2-41)

Engine or gas generation	2150. lb
Tank and systems	1050. lb
Electrical distribution	3500. lb
Hydraulic and pneumatic	1100. lb

The electrical and hydraulic/pneumatic system weight are very nearly equal for the WAATS and HST analyses. The other items may be included in the engine weight in the WAATS program.

**Avionics:** The HST Avionics weight is broken down into (ref. 8, page 2-39)

Guidance and navigation	800. lb
Instrumentation	400. lb
Communications	2000. lb

The WAATS estimate is based on the correlation curve shown in Fig. 3.8-1 of ref. 5. The correlation is not good and the data is for much lighter aircraft than the one being considered here. Therefore, the WAATS estimate, which is more than twice the HST value, may not be realistic.

Crew Systems and Payload Provisions: The WAATS Crew Systems weight includes the equipment and personnel environment control system, crew compartment insulation, personnel accommodations, fixed life support equipment, emergency equipment, crew station controls and panels (ref. 5, p. 75). In ref. 8, page 2-41, the Payload Provisions are stated to be a substantial weight item, but are not described. However, in ref. 23, pages 8-9, Personnel Provisions are broken down into accommodations for personnel, fixed life support, furnishings and cargo handling, emergency equipment, and controls and panels. The equipment descriptions are similar, but the HST weight item is over ten times the WAATS weight item. The large discrepancy may be due to the fact that the vehicle of ref. 23 has a payload of 200 passengers plus cargo, while no provisions are made in the WAATS analysis for passenger accommodations.

Payload: The payload is the same in both analyses.

Crew and Residuals: The Crew and Trapped Fuel weights are summed to obtain the WAATS weight item. The HST weight item is listed as Personnel, Residuals and Prime Power Reserve, but the term Prime Power Reserve is not explained. The resulting weights differ by approximately thirty-seven percent.

Propellants: The WAATS Main Propellant and Reserve Propellants were adjusted to give the same total weight as the HST analysis (see the Design Data section).

Inflight Losses: The WAATS weight coefficient was chosen to make the WAATS weight item equal to the HST weight item.

Empty Weight: Since there is no Design Reserve, the Dry and Empty Weights are the same in the WAATS Weight Statement. This weight is sixteen percent lower than the HST Dry Airplane weight. However, if the major weight items--the Aerodynamic Surfaces, the Body Structure and the Engines--are compared, the difference in weights is only six percent. Thus the system weights account for the majority of the Empty Weight difference.

Landing Weight: Without an Attitude Control System, the WAATS Landing and Entry Weights are the same and within twelve percent of the HST Wet Airplane and Payload Weight.

Takeoff Weight: The difference between the Takeoff and Landing Weights for the two analyses is the same, so the final difference is reduced to eight percent.

In general, the results of the WAATS analysis are considered to be good. Since the HST weights are also estimates, their accuracy is open to question; although they are based on a much more detailed study than was possible for the WAATS analysis. There are a number of areas where the WAATS equations and their coefficients and exponents should be thoroughly reviewed. The systems area should be given special attention. This would be much more feasible if the data base discussed previously were available. It should also be noted that as a design develops, and more accurate data becomes available, the WAATS program can be used to update the weight estimate very rapidly and inexpensively.

#### CONCLUSIONS

Of the three methods of weight prediction--fixed-fraction, statistical correlation and point stress analysis--the statistical correlation method is probably the best for preliminary design. The modified WAATS program is considered to be a good tool for feasibility studies of hypersonic aircraft; however, some areas need further investigation. The specific areas, primarily systems weights, are noted in the comparison of the WAATS results with the HST weights. Further development of this, and other, weight estimation programs would benefit from the availability of a comprehensive data base of component weights.

## APPENDIX

### THE WAATS EXAMPLE PROBLEM

The example problem in ref. 5 was not used as the principal example in this report because very few details were given on the vehicle for which the weight was being estimated. However, in order to verify that the modified program gives the same results as the original program, the example is presented on the following pages. The completed Input Data Forms, an Input Data Listing and the printed output are presented. Note that there are more non-zero weight coefficients printed than in ref. 5 because of the specified values in the modified program. All of the weights are within one pound of the values given in ref. 5.

## WAATS INPUT DATA - DESIGN DATA

## VEHICLE DESIGNATION WAATS EXAMPLE

VEHICLE DESIGNATION	1			2			3		
	3	2	1	2	1	2	3	2	1
ICNG	2								
ICRY	2								
ISHAPE	2								
ACIN	1.0								
AICAPT	0.0								
ARATIO	0.0								
CNEW	2.0								
DH	0.0								
DN	1.0								
ELBCDV	0.0								
ELNLET	0.0								
FLRAMP	0.0								
ENGINS	2.0								
FCIMLK	1.0								
GENFCY	1.0								
GSPAN	0.0								
IMCUDY	1.0								
UF	6.0								
UFACS	0.0								
PCHAN	1000.0								
PHIGH	176.0								
PLNW	46.0								
QMAX	0.0								
SBODY	0.0								
SFAIR	0.0								

80.

350.

22.

141.

20.

2500.

32800.

# HATS INPUT DATA - DESIGN DATA

IENG	ICRY	ISHAPE	1						2						3	
			1		2				1		2				1	2
			1	2	1	2	1	2	1	2	1	2	1	2		
SFUTK	0.0		XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX	*		
SHDRZ	0.0		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	1.		
SUXIK	0.0		XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX				*		
STPS	0.0													42300.		
STSPAN	0.0													93.71		
SVEPT	0.0		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	1380.		
SWING	0.0		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	11579.		
TANKS	1.0				XXXXXXXXXX		XXXXXXXXXX				XXXXXXXXXX		XXXXXXXXXX	XXXXXXXXXX		
THRLST	0.0													4.7E6		
TPQUT	0.0		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX	11.46		
TYTAIL	1.25													*		
VFUTK	0.0													143200.		
VJATK	0.0		XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX	53100.		
WAREF	0.0								XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX		
VLANDJ	0.0													900000.		
WPAYLO	0.0													40000.		
UPMAIN	0.0													4.4E6		
WTUIN	0.0													7.0E6		
XIPLET	1.0													*		
XLV	4.0													3.75		

## VEHICLE DESIGNATION

[illegible]



# HAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPORTS

IFRG	1						2						3		
	1			2			1			2			2		
	1	2		1	2		1	2		1	2		1	2	
ICPV															
ISHAPE															
27	0.0														*
28	0.00766														0.0076
29	0.00033														*
30	0.5														*
31	130.0														700.
32	1782.63														XXXXXXXXXX
33	0.003														XXXXXXXXXX
34	1994.53														XXXXXXXXXX
35	0.0032														XXXXXXXXXX
36	0.53														XXXXXXXXXX
37	0.0														0.
38	1.25														*
39	0.0														0.
40	0.59														*
41	0.0														*
42	0.23														*
43	0.0														*
44	0.0														0.0022
45	0.0														0.5
46	0.0														*
47	0.0														0.0043
48	0.0														0.5
49	0.0														*

NAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

IENG	ICRV	ISHAPE	1						2						3		
			1		2				1		2				2		3
			1	2	1	2	1	2	1	2	1	2	1	2	1	2	
50		0.45	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX				0.
51		2.45	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX				0.
52		0.0	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX				*
53		4.345															*
54		1.0															*
55		0.0	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX				*
56		0.0	XXXXXXXXXX	XXXXXXXXXX			XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX		XXXXXXXXXX				*
57		78.5															0.
58		0.079															*
59		0.0															*
60		0.323															0.
61		0.0															*
62		0.0															*
63		0.0															*
64		0.10															0.
65		0.0															*
66		1.167															0.
67		0.0															*
68		2.64															0.
69		0.0															*
70		66.37															0.
71		0.0															6600.
72		220.0															*

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# WAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

IENG	ICRV	ISHAPE	1						2						3					
			1			2			1			2			1			2		
			1	2		1	2		1	2		1	2		1	2		1	2	
73		0.0																	1330.	
74		0.0																	*	
75		0.0																	2675.	
76		0.0																	*	
77		0.0																	*	
78		0.608	XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	*	
80		0.0																	*	
81		1.0																	*	
82		0.1	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	XXXXXXXX	
83		0.0	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	XXXXXXXX	
84		0.0																	0.004	
85		0.0																	0.5	
86		0.0	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	0.004	
87		0.0	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	*	
88		1.09	XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	1.1	
90		1.0	XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	*	
91		0.0																	XXXXXXXX	
92		0.0																	0.0075	
93		0.0																	*	
94		0.0	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	0.0075	
95		0.0	XXXXXXXX	XXXXXXXX		XXXXXXXX	XXXXXXXX		XXXXXXXX			XXXXXXXX			XXXXXXXX			XXXXXXXX	*	
96		0.0																	*	
97		0.0																	*	

[illegible]

MAATS INPUT DATA - WEIGHT COEFFICIENTS AND EXPONENTS

ITEM	1						2						3	
	1			2			1			2			2	
	1	2		1	2		1	2		1	2		1	2
ICRY														
ISHAPE														0.334
122		0.0												1.0
123		1.0E-6												0.01375
124		0.0												1.0
125		1.0E-6												0.1095
126		0.0												1.4425
127		1.0E-6												*
128		0.0												0.0114
129		0.0												0.637
130		0.0												*
131		0.0												0.534
132		0.0												*
133		0.0												0.05
134		0.0												

# INPLT DATA - WAATS EXAMPLE

```

EINWAP ARATIO=80.0,
CH=60000.0,
DM=4.5,
ELBODY=350.0,
ENGINS=22.0,
GSPAN=141.0,
HBCDY=20.0,
GMAX=2500.0,
SBCDY=32800.0,
SHCRZ=1.0,
STPS=42300.0,
STSPAN=93.71,
SVERT=1380.0,
SWING=11579.0,
TANKS=2.0,
THRUST=470000.0,
TROOT=11.46,
VFUTK=143200.0,
VOXTK=53100.0,
WAREF=122.7,
WLANDI=900000.0,
WPAYLD=40000.0,
WPMAN=4400000.0,
WTCIN=7000000.0,
XLF=3.75,
AC(1)=0.0,
AC(4)=4.2,
AC(6)=0.0,
AC(14)=1.2378,
AC(15)=0.0,
AC(17)=0.0,
AC(19)=0.004,
AC(21)=2.3,
AC(25)=0.0,
AC(26)=0.00916,
AC(28)=0.0076,
AC(31)=700.0,
AC(36)=0.0,
AC(38)=0.0,
AC(44)=0.0022,
AC(45)=0.5,
AC(47)=0.0043,
AC(48)=0.5,
AC(50)=0.0,
AC(51)=0.0,
AC(57)=0.0,
AC(60)=0.0,
AC(64)=0.0,
AC(66)=0.0,
AC(68)=0.0,
AC(70)=0.0,
AC(71)=6600.0,
AC(72)=0.0,
AC(73)=1330.0,
AC(75)=2675.0,
AC(84)=0.004,
AC(85)=0.5,

```

INPUT DATA - WAATS EXAMPLE

AC(86)=0.004,  
AC(89)=1.1,  
AC(92)=0.0075,  
AC(94)=0.0075,  
AC(98)=0.12,  
AC(102)=0.0001,  
AC(115)=0.015,  
AC(116)=0.004,  
AC(117)=2400.0,  
AC(118)=0.584,  
AC(121)=1.124,  
AC(122)=0.334,  
AC(123)=1.0,  
AC(124)=0.01375,  
AC(125)=1.0,  
AC(126)=0.1095,  
AC(127)=1.4425,  
AC(129)=0.0114,  
AC(130)=0.637,  
AC(132)=0.534,  
AC(134)=0.05,&END





# NON-ZERO WEIGHT COEFFICIENTS

AC( 4) = 4.20000  
 AC( 14) = 1.23780  
 AC( 19) = .400000E-02  
 AC( 21) = 2.30000  
 AC( 26) = .916000E-02  
 AC( 28) = .760000E-02  
 AC( 29) = .330000E-03  
 AC( 30) = .500000  
 AC( 31) = 700.000  
 AC( 32) = 1782.63  
 AC( 33) = .300000E-02  
 AC( 34) = 1994.53  
 AC( 35) = .320000E-02  
 AC( 40) = .590000  
 AC( 42) = .230000  
 AC( 44) = .220000E-02  
 AC( 45) = .500000  
 AC( 47) = .430000E-02  
 AC( 48) = .500000  
 AC( 53) = 4.34500  
 AC( 54) = 1.00000  
 AC( 58) = .790000E-01  
 AC( 71) = 6600.00  
 AC( 73) = 1330.00  
 AC( 75) = 2675.00  
 AC( 78) = .608000  
 AC( 81) = 1.00000  
 AC( 82) = .100000  
 AC( 84) = .400000E-02  
 AC( 85) = .500000  
 AC( 86) = .400000E-02  
 AC( 89) = 1.10000  
 AC( 90) = 1.00000  
 AC( 92) = .750000E-02  
 AC( 94) = .750000E-02  
 AC( 98) = .120000  
 AC(101) = .795000  
 AC(102) = .100000E-03  
 AC(104) = .316000  
 AC(106) = 117.350  
 AC(107) = .294000  
 AC(110) = .100000E-05  
 AC(111) = .903000  
 AC(112) = 1.00000  
 AC(113) = 1.00000  
 AC(114) = .361000  
 AC(115) = .150000E-01  
 AC(116) = .400000E-02  
 AC(117) = 2400.00  
 AC(118) = .584000  
 AC(120) = .100000E-05  
 AC(121) = 1.12400

NON-ZERO WEIGHT COEFFICIENTS

AC(122) = .334000  
AC(123) = 1.00000  
AC(124) = .137500E-01  
AC(125) = 1.00000  
AC(126) = .109500  
AC(127) = 1.44250  
AC(129) = .114000E-01  
AC(130) = .637000  
AC(132) = .534000  
AC(134) = .500000E-01

# DESIGN DATA

## WETTED AREAS

GROSS BODY	32800.00
FUEL TANKS	0.0
OXIDIZER TANKS	0.0

## PLAN AREAS

WING	11579.00
VERTICAL SURFACES	1380.00
HORIZONTAL SURFACES	1.00
FAIRINGS	0.0
THERMAL PROTECTION SYSTEM	42300.00

## DIMENSIONAL DATA

WING GEOMETRIC SPAN	141.00
WING STRUCTURAL SPAN	93.71
WING THICKNESS AT THEORETICAL ROOT	11.46
TOTAL INLET CAPTURE AREA	0.0
ROCKET ENGINE AREA RATIO	80.00
TOTAL INLET LENGTH	0.0
TOTAL RAMP LENGTH	0.0
BODY LENGTH	350.00
BODY HEIGHT	20.00
FUEL TANK VOLUME	143200.00
OXIDIZER TANK VOLUME	53100.00

## ENGINE DATA

ENGINE TYPE	ROCKET
NUMBER OF ENGINES	22.00
THRUST OF ONE ENGINE	470000.00
THRUST SCALING FACTOR	1.00
NUMBER OF INLETS	1.00
REFERENCE ENGINE AIRFLOW	122.70
ROCKET ENGINE CHAMBER PRESSURE	1000.00
TURBORAMJET INLET PRESSURE (UPPER)	176.00
TURBORAMJET INLET PRESSURE (LOWER)	46.00

## WEIGHTS

PAYLOAD	40000.00
MAIN IMPULSE PROPELLANT	4400000.00
ESTIMATED TAKEOFF WEIGHT	7000000.00
ESTIMATED LANDING WEIGHT	900000.00

**D E S I G N   C A T A**

**OTHER DESIGN DATA**

NUMBER OF CREW	2.00
DESIGN ALTITUDE	60000.00
DESIGN MACH NUMBER	4.50
MACH NUMBER FACTOR	1.00
GEOMETRICAL CUT OF ROUND FACTOR	1.00
OXIDIZER TO FUEL MIXTURE RATIO	6.00
ACS OXIDIZER TO FUEL MIXTURE RATIO	0.0
MAXIMUM DYNAMIC PRESSURE	2500.00
NUMBER OF FUSELAGE FUEL TANKS	2.00
TAIL TYPE COEFFICIENT	1.25
ULTIMATE LOAD FACTOR	3.75
PROPELLANT TYPE	CRYOGENIC
SHAPE	AIRCRAFT

# MASS ITERATION

NO	DRY WEIGHT	EMPTY WEIGHT	LANDING WEIGHT	ENTRY WEIGHT	TAKEOFF WEIGHT
1	683039.	765004.	840141.	885141.	5320341.
2	676188.	757330.	832456.	876713.	5311913.
3	674975.	755972.	831092.	874927.	5310127.

# W E I G H T   S T A T E M E N T

AERODYNAMIC SURFACES		78482.
WING	66539.	
VERTICAL SURFACES	11943.	
HCRIZONTAL SURFACES	0.	
FAIRINGS	0.	
BODY STRUCTURE		201534.
BASIC STRUCTURE	40600.	
SECONDARY STRUCTURE	0.	
THRUST STRUCTURE	41360.	
INTEGRAL FUEL TANKS	91218.	
INTEGRAL OXIDIZER TANKS	28355.	
ENVIORNMENTAL PROTECTION SYSTEM		97290.
INSULATION	97290.	
CCVER PANELS	0.	
LAUNCH AND RECOVERY SYSTEMS		41341.
LAUNCH SYSTEM	0.	
LANDING GEAR	41341.	
MAIN PROPULSION SYSTEM		193097.
ENGINES	124504.	
ENGINE MOUNTS	1034.	
FUEL TANKS	0.	
OXIDIZER TANKS	0.	
FUEL TANK INSULATION	0.	
OXIDIZER TANK INSULATION	0.	
FUEL SYSTEM	22923.	
OXIDIZER SYSTEM	44637.	
PROPELLANT PRESSURIZATION SYST	0.	
INLET SYSTEM	0.	
ORIENTATION AND SEPARATION SYSTEMS		26457.
GIMBAL SYSTEM	0.	
ATTITUDE CONTRCL SYSTEM	12055.	
ATTITUDE CONTOL SYSTEM TANKAGE	0.	
AERODYNAMIC CONTRCL SYSTEM	14402.	
SEPARATION SYSTEM	0.	
POWER SUPPLY		27499.
ELECTRICAL SYSTEM	17505.	
HYDRAULIC/PNEUMATIC SYSTEM	9995.	
AVIONICS SYSTEM		6600.
CREW SYSTEMS		2675.
DRY WEIGHT		674975.

# WEIGHT STATEMENT

DRY WEIGHT		674975.
DESIGN RESERVE	80997.	
EMPTY WEIGHT		755972.
PAYLOAD	40000.	
CREW	1330.	
RESIDUAL PROPELLANTS		33132.
TRAPPED FUEL	4733.	
TRAPPED OXIDIZER	28399.	
LANDING WEIGHT		831092.
ATTITUDE CONTROL SYSTEM PROPELLANTS		43836.
FUEL	43836.	
OXIDIZER	0.	
ENTRY WEIGHT		874927.
MAIN PROPELLANTS		4400000.
FUEL	628571.	
OXIDIZER	3771428.	
RESERVE PROPELLANTS		17600.
FUEL	2515.	
OXIDIZER	15086.	
INFLIGHT LOSSES		17600.
TAKEOFF WEIGHT		5310127.

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